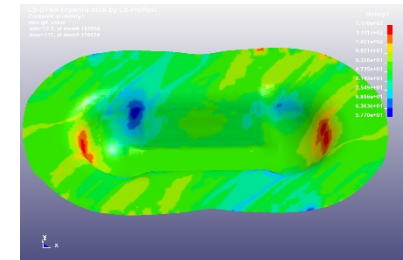
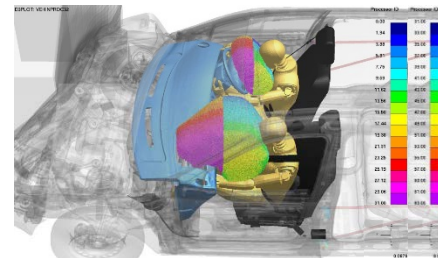
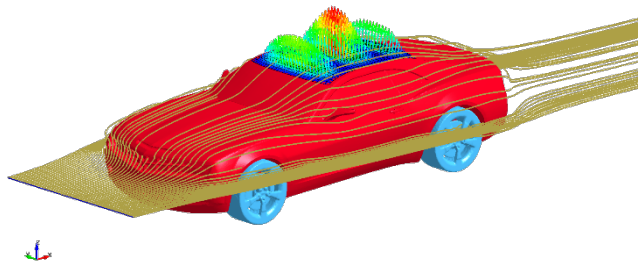


# Recent and Ongoing Developments in LS-DYNA®

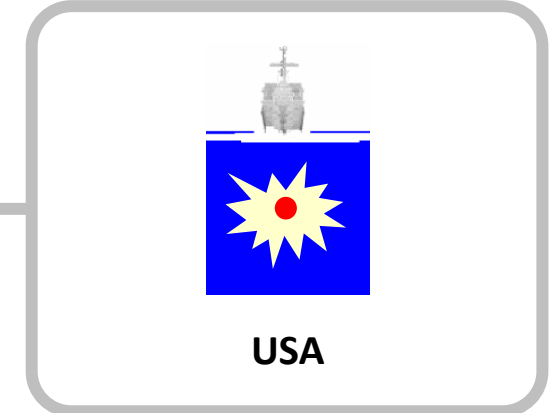
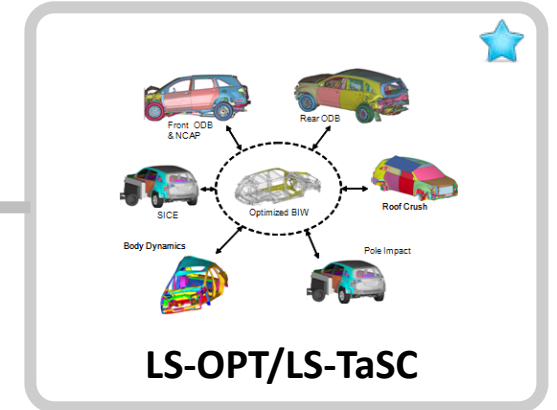
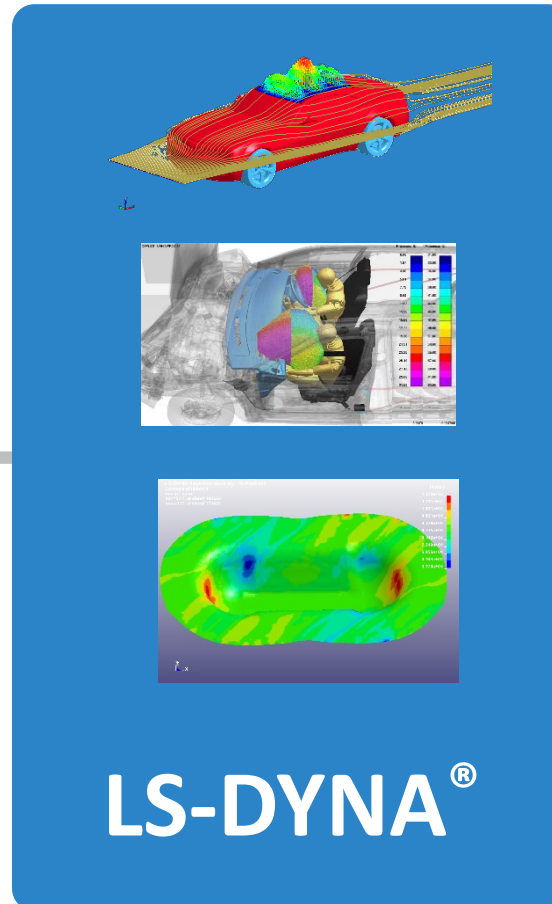
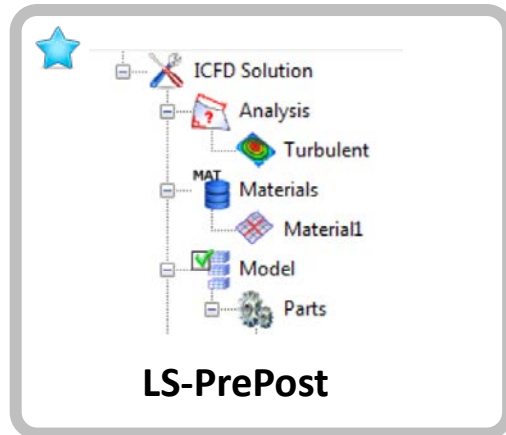


John O. Hallquist, Pierre L'Eplattenier, Facundo Del Pin, Jason Wang,  
Edouard Yreux, John Zhao, Yun Huang, Isheng Yeh, Nielen Stander



Nordic LS-DYNA Users Conference  
Göteborg, Sweden  
October 18, 2018

## Multi-Physics Solver, Pre-and-Post Processor, Optimization, and Library of Validated Dummies and Barriers



# LS-DYNA | One Code, One Model



## Single Model for Multiple Disciplines – Manufacturing, Durability, NVH, Crash, and FSI

### Multi-Physics

Structure + Fluid + EM + Heat Transfer

### Multi-Stage

Implicit + Explicit ...

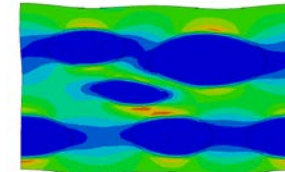
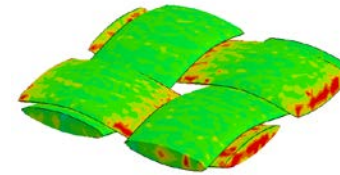
### Multi-Formulations

Linear + Non-Linear + Fatigue ...

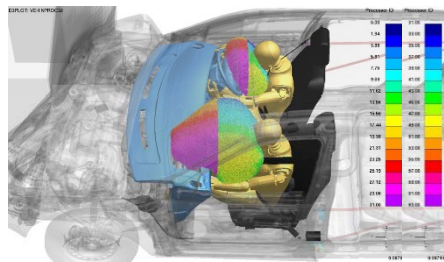
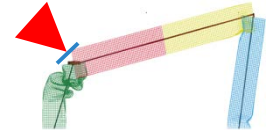
### Multi-Scale

Failure predictions, i.e., spot welds, composites, crystal plasticity

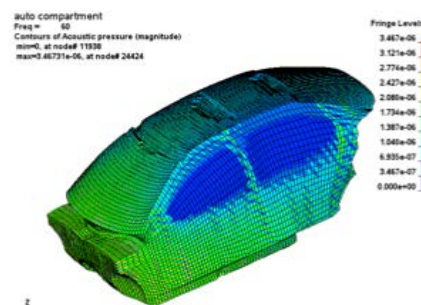
Composites  
(C.-T. Wu)



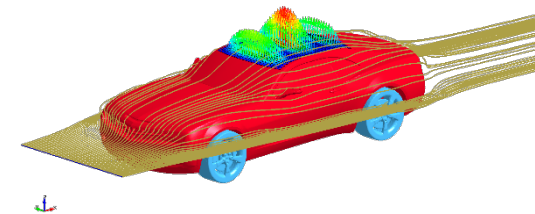
Crushable beam (Yeh)



Crash



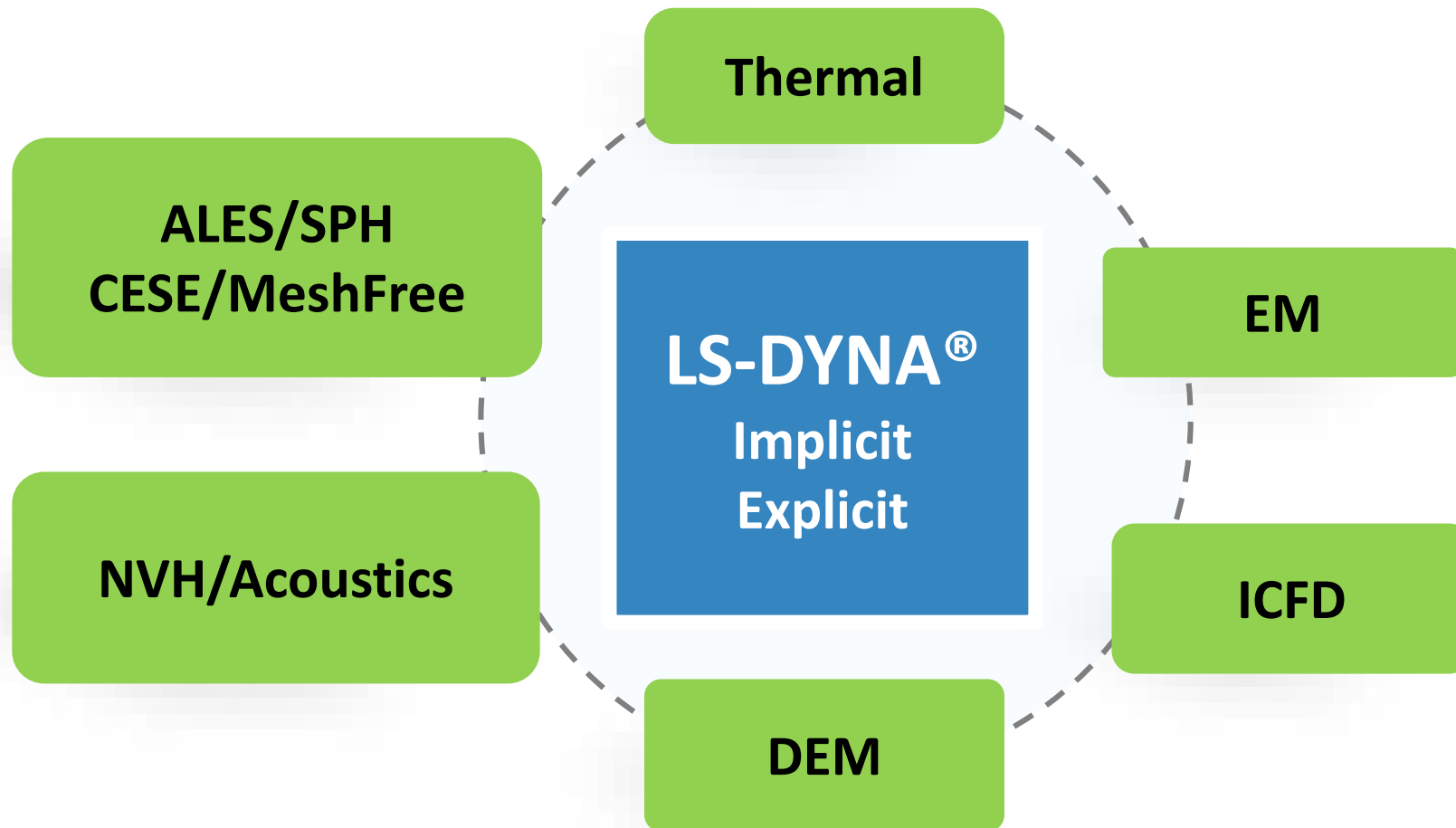
NVH



Structure + Fluid

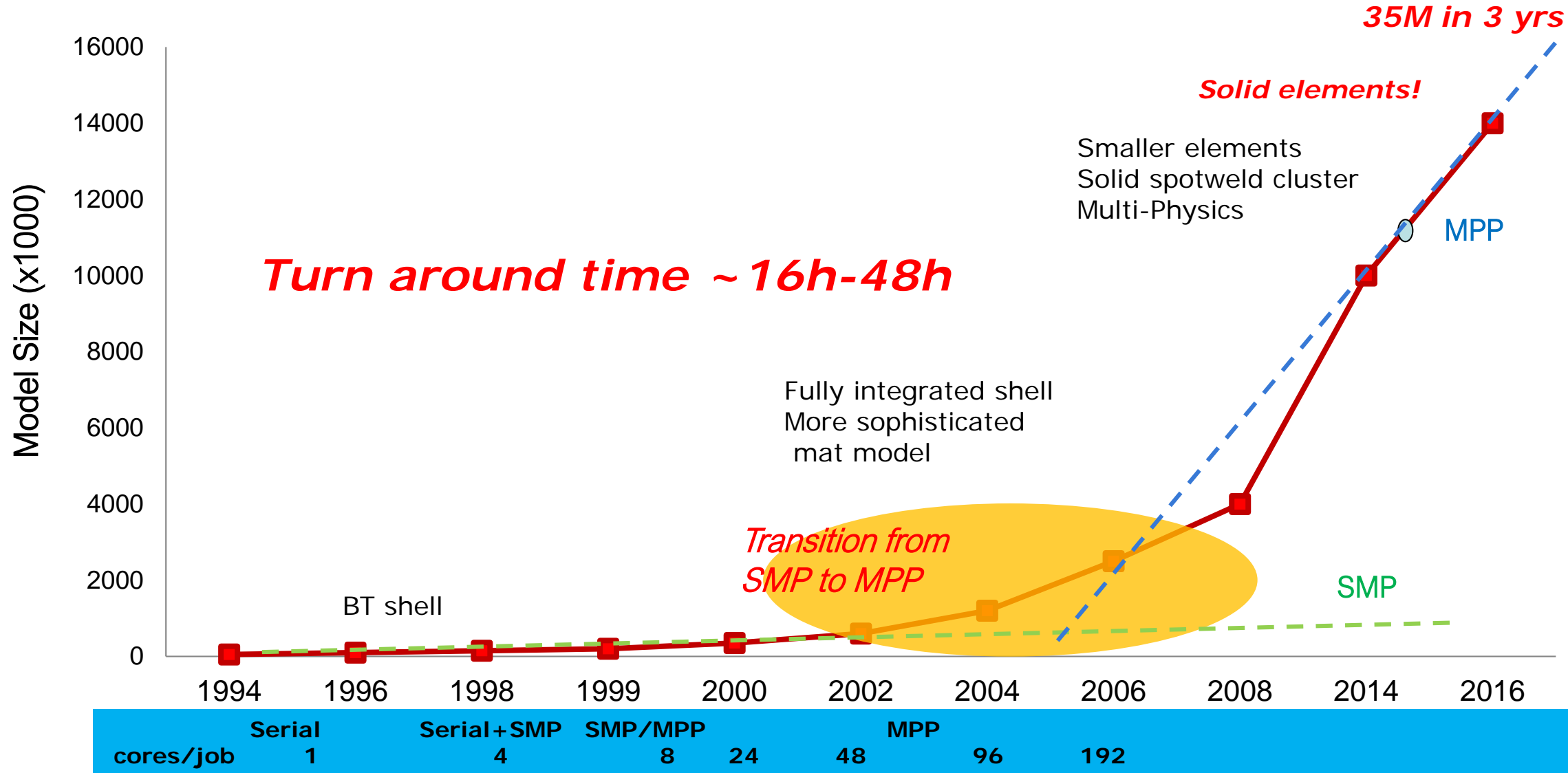
# LS-DYNA | Strongly Coupled Multi-Physics Solver

Computers capable of multi-physics simulations are becoming affordable.  
Scalability is rapidly improving for solving multi-physics problems





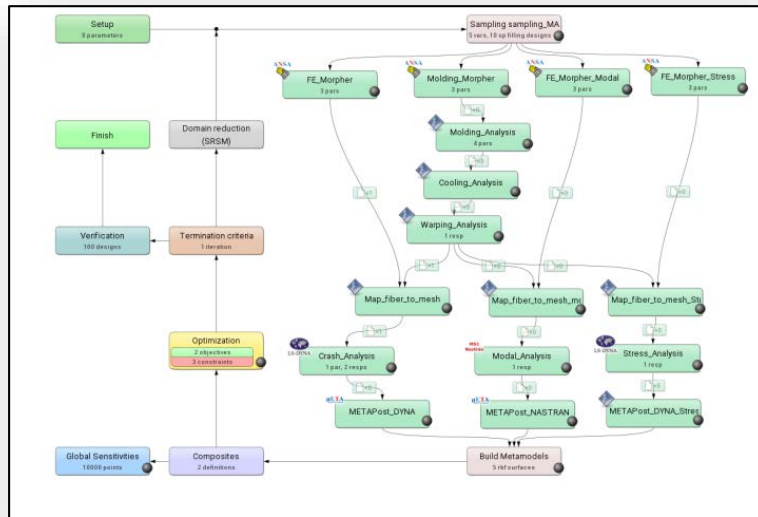
# Model size for Safety Analysis



# LS-OPT® | Optimization, Probabilistic Analysis & System Calibration

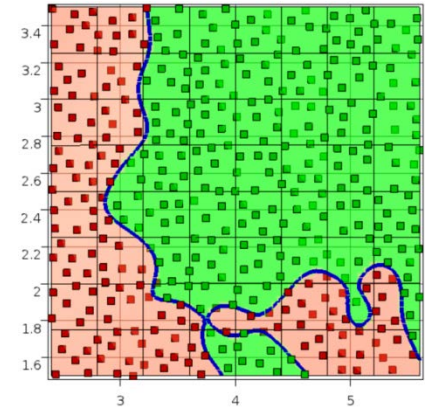
LS-DYNA® can be incorporated in a *multi-stage, multi-case, multi-level* process

- **Multi-case, Multi-stage, Multi-level**



- **Statistics & Uncertainty**

- Robust Design
- Sensitivity Analysis
- LS-DYNA® Statistics
- Outlier Analysis
- *Classification*



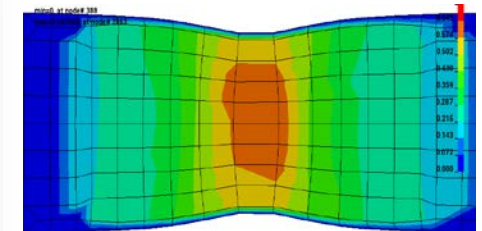
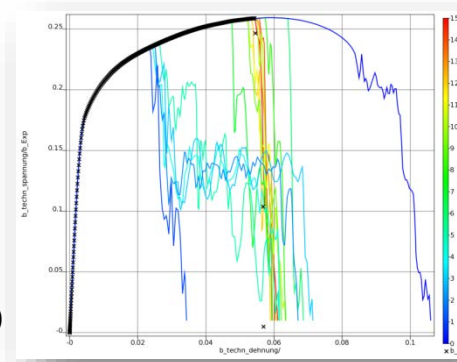
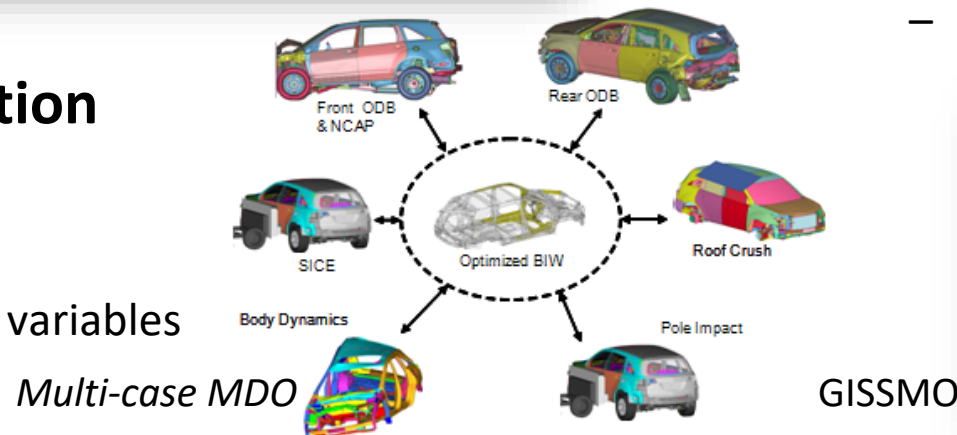
SVM Classifier

- **Material Calibration**

- Hysteresis: Loading-Unloading
- *Noise handling e.g. GISSMO*
- *Full-field Calibration w. Digital Image Correlation*

- **Optimization**

- MDO
- MOO
- Discrete variables



Digital Image mapping

# Outline

## **Electromagnetics**

Pierre L'Eplattenier

## **ICFD**

Facundo Del Pin

## **Particle Methods**

Jason Wang

## **Implicit Analysis**

Roger Grimes

## **Composites**

John Zhao

## **Acoustics and Fatigue Analysis**

Yun Huang

## **Crashworthiness: Beams**

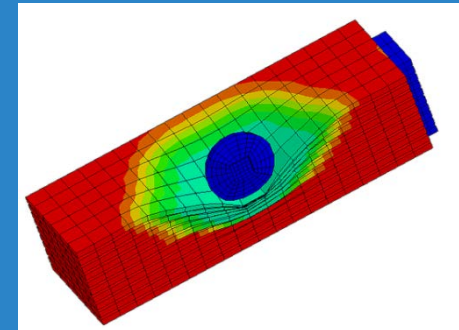
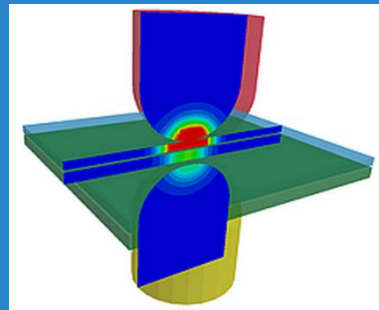
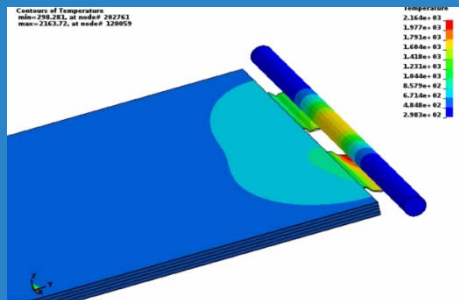
Isheng Yeh

## **Optimization**

Nielen Stander

# Electromagnetics

Dr. Pierre L'Eplattenier



# Outline

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- Battery abuse
- Resistive spot welding

# Battery – Distributed Randles circuit model

## Electro-chemistry in the electrodes simulated by equivalent electrical circuits (Randles circuits)

Vehicle



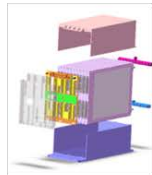
Dual-Packs



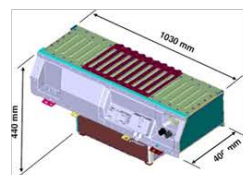
Cell



Module

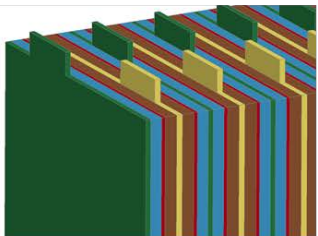


Pack

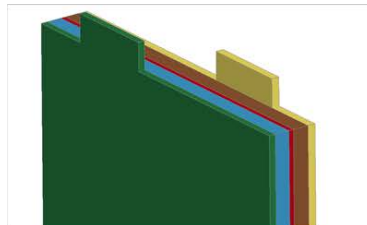


180 $\mu$ m

Cell (zoomed in z)

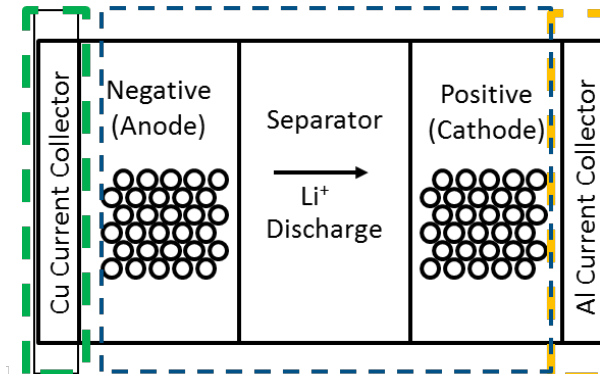
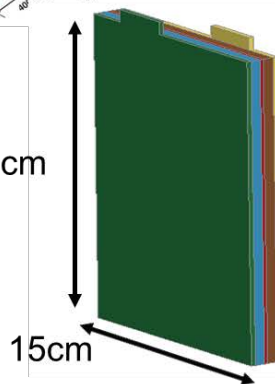


Unit cell (zoomed in z)

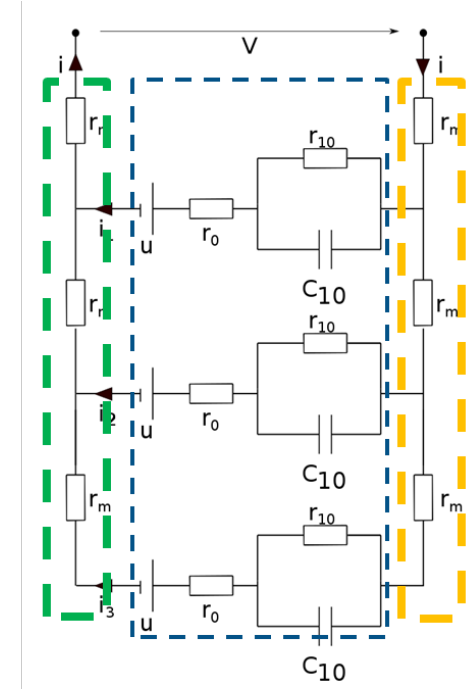


20cm

15cm



- Current collectors transport electrons to/from tabs; modeled by resistive elements
- Jelly roll (anode – separator – cathode) transports Li<sup>+</sup> ions; modeled with Randle circuit



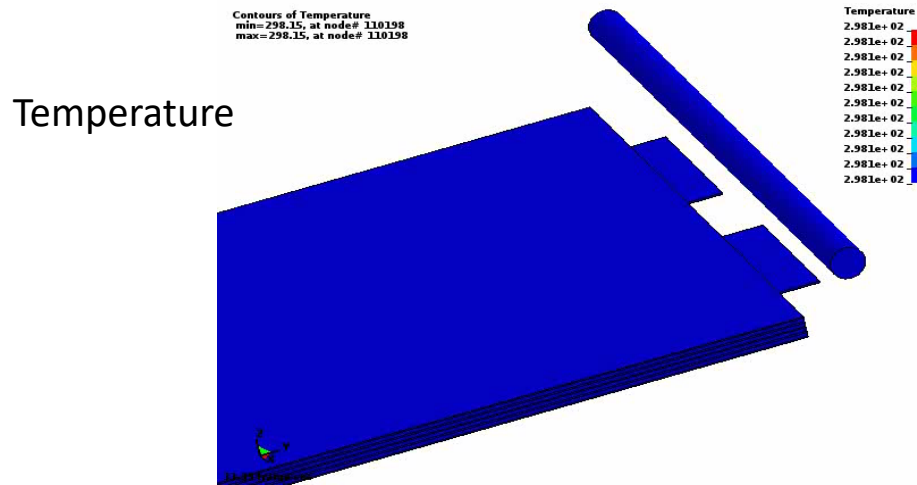
$r_0$ : Ohmic & kinetic

$r_{10}$  &  $c_{10}$ : Diffusion

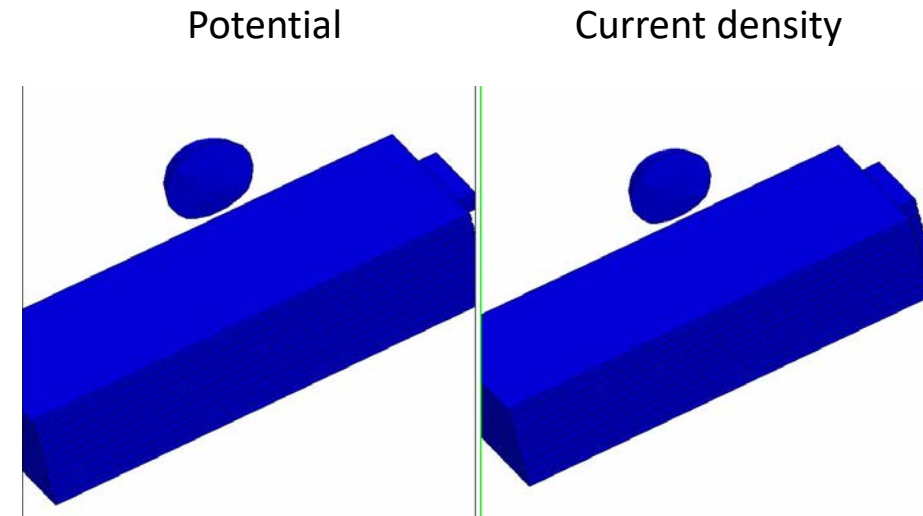
$u$ : Equilibrium voltage (OCV)

$r_m$ : Current collectors

- Battery abuse simulations on cells, modules, packs
- Pouch cells, cylindrical cells available, soon prismatic cells
- Coupled with mechanical and thermal solvers
- Solid, shells and composite thick shells
- External and internal shorts
- Battery packaging application in LS-PrePost



External short  
5 cells module



Internal short  
10 cells module

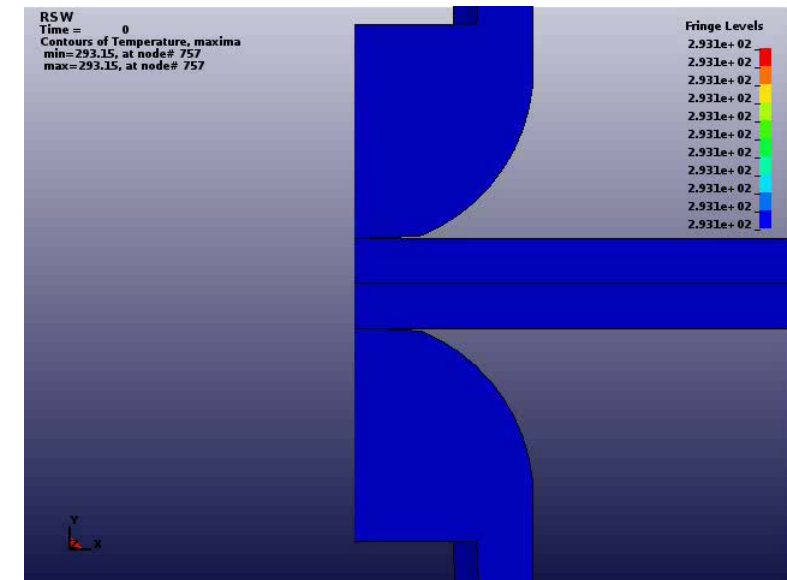
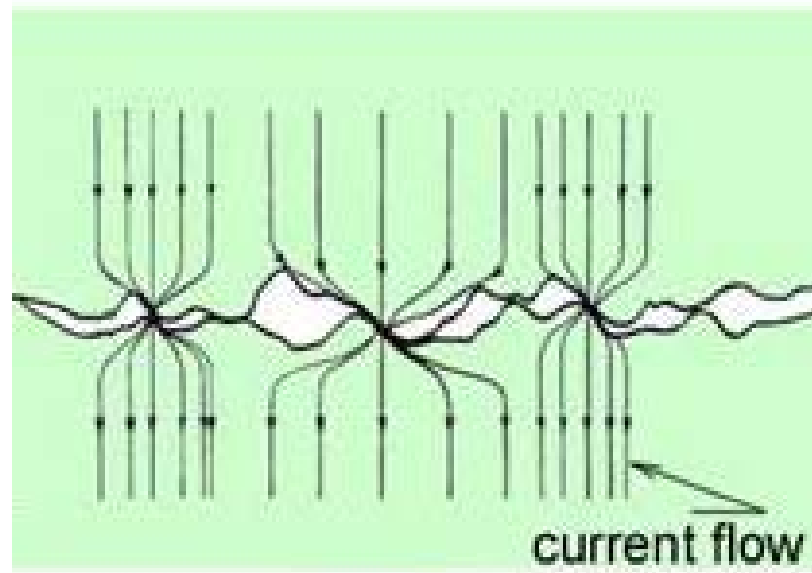
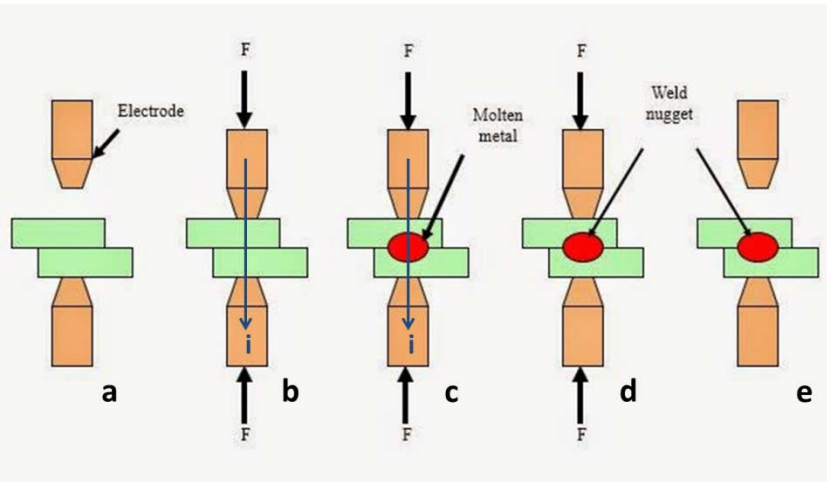


# Resistive spot welding

## New model in LS-DYNA for local contact resistance depending on local parameters, using \*DEFINE\_FUNCTION

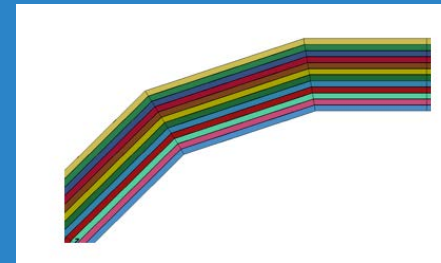
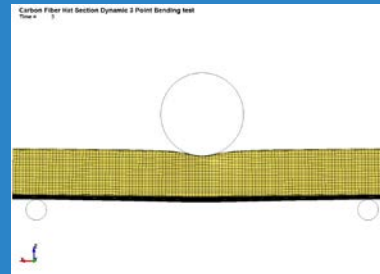
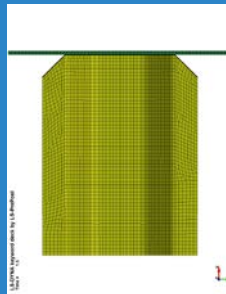
Electrodes on each sides of sheets  
using Pressure and Current Flow  
resulting in molten weld nugget

$$r(T, P) = r_0 \left( \frac{p - p_k}{p_0 - p_k} \right)^{\varepsilon_p} \cdot \left( \frac{T - T_{\text{lim}} + (293,15 \text{ K} - T) \cdot 2^{-\frac{1}{\varepsilon_T}}}{293,15 \text{ K} - T_{\text{lim}}} \right)^{\varepsilon_T}$$



# Composites

Dr. John Zhao



# Continuous long fiber compression molding

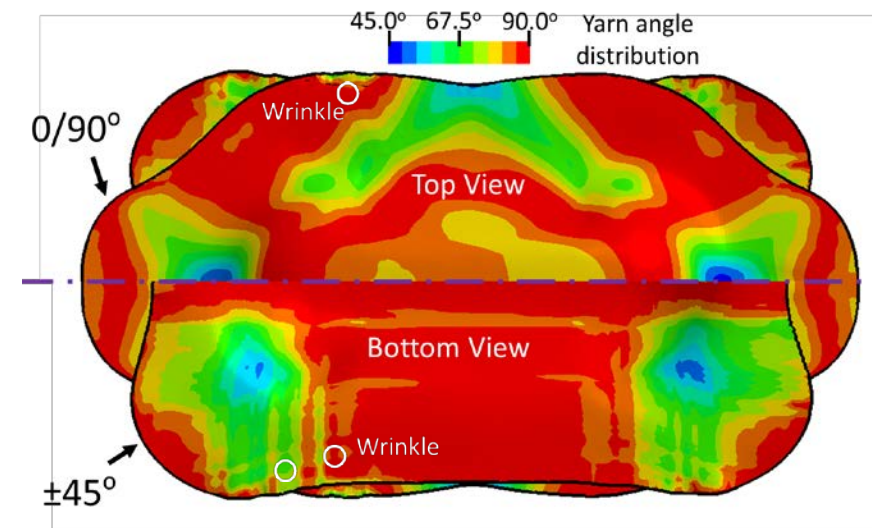
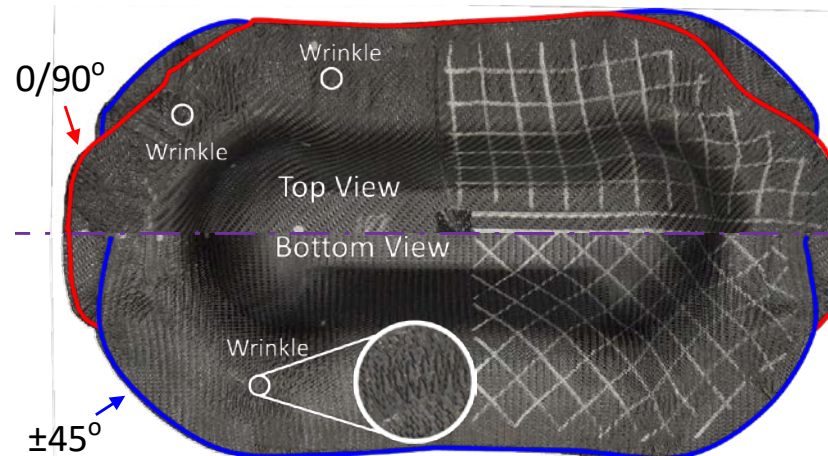


Transfer the fiber orientation from the manufacturing process to the crash analysis.

- MAT\_277 developed by DOW and Ford for resin curing process. Curing curve determines mechanical properties.
- MAT\_278 micro mechanics model for woven prepreg compression molding. Deformation gradient to update angle changes.
- MAT\_293 non-orthogonal model for compression molding developed . Easy integration of test results.
- For woven long fiber composite, fiber angle after forming is crucial information for accurate prediction of crash performance

Layers differ in:

- Geometry
  - Drawing distance
- Sliding between layers



# ICFD

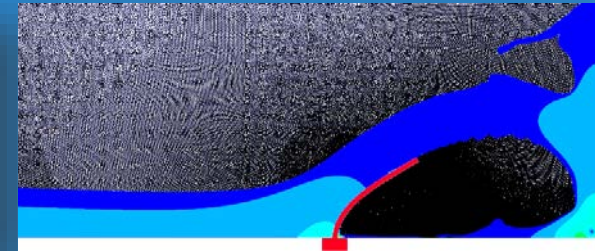
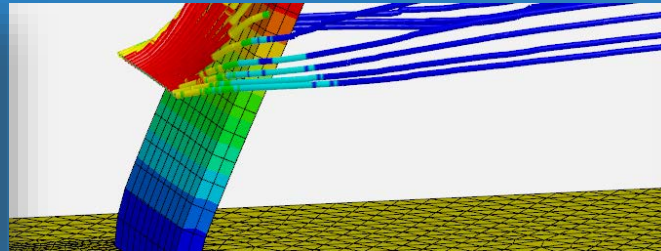
## Recent Developments

Facundo Del Pin

Iñaki Çaldichoury

Rodrigo R. Paz

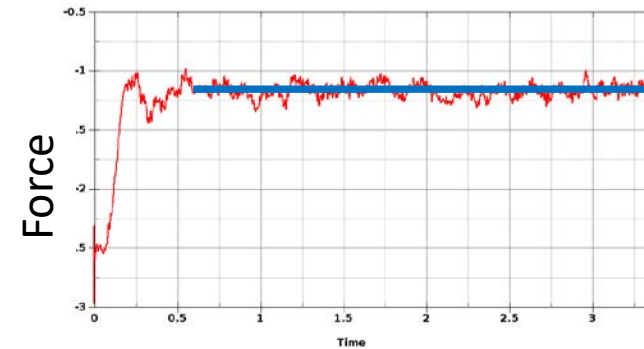
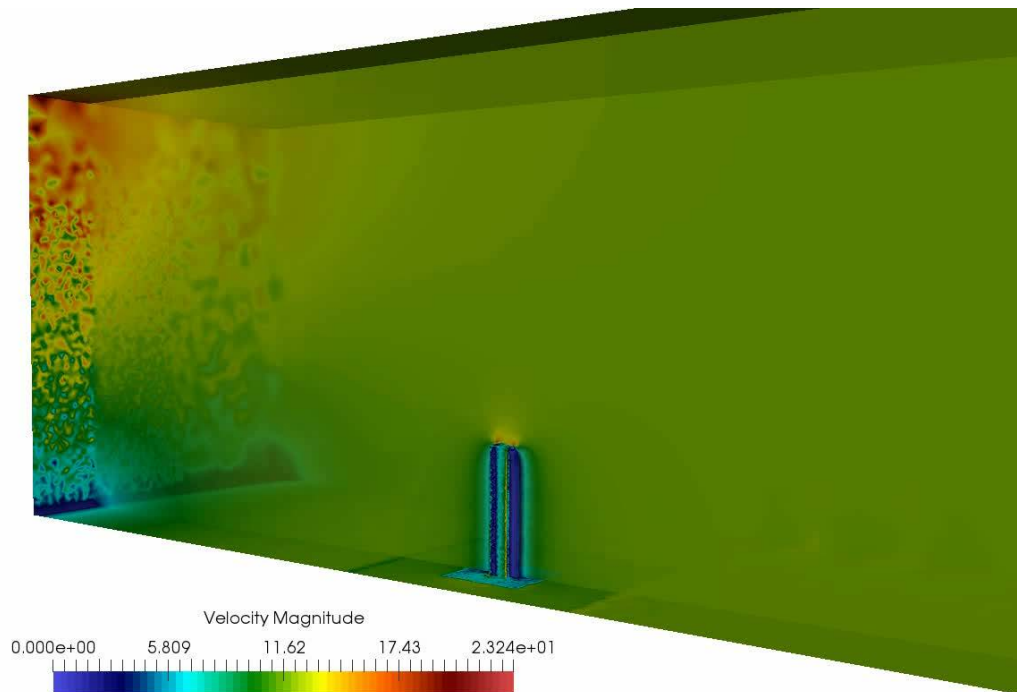
Chien-Jung Huang



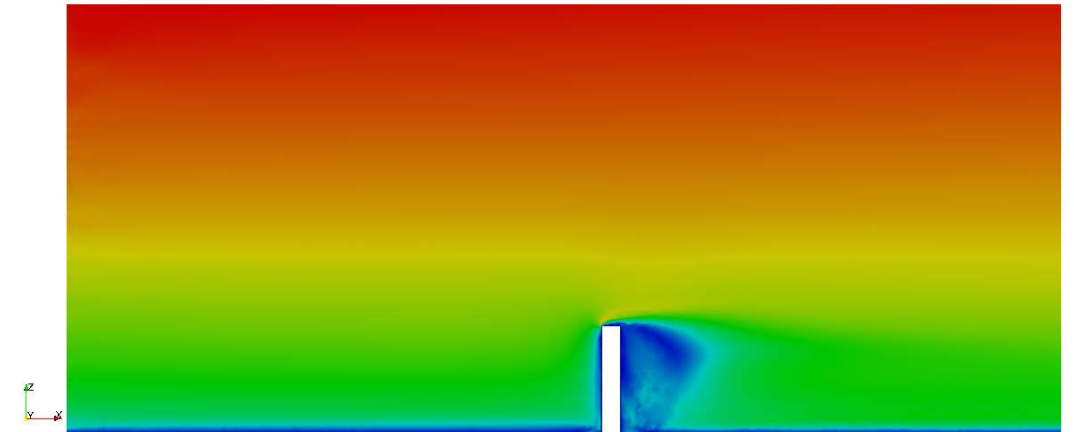
# Steady State for Fluid-Structure Interaction

Delpin, Caldichoury, Paz, Wang

The steady state solver or the potential flow solver allow for a fast linearization of Fluid Structure Interaction (FSI) and/or Conjugate Heat transfer (CH) problems



Steady state analysis allows engineers to study physical problems in a time average fashion.



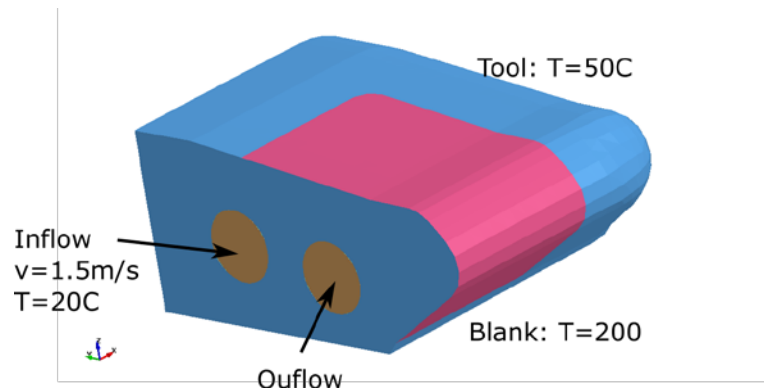
These simulations provide valuable insight faster which is useful for prototyping.



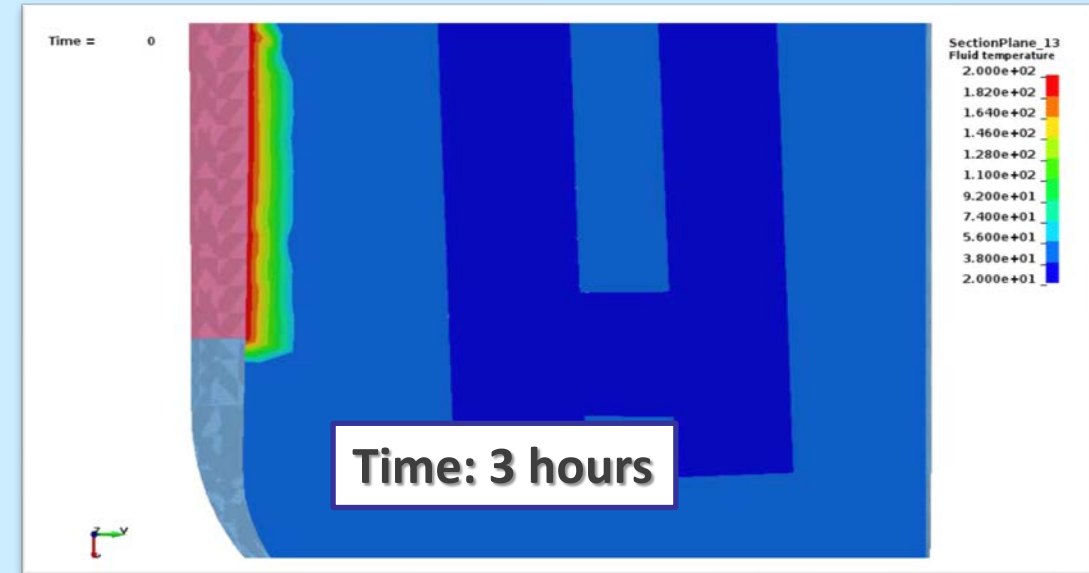
# Conjugate Heat: Cooling problem

Delpin, Caldichoury, Paz, Wang

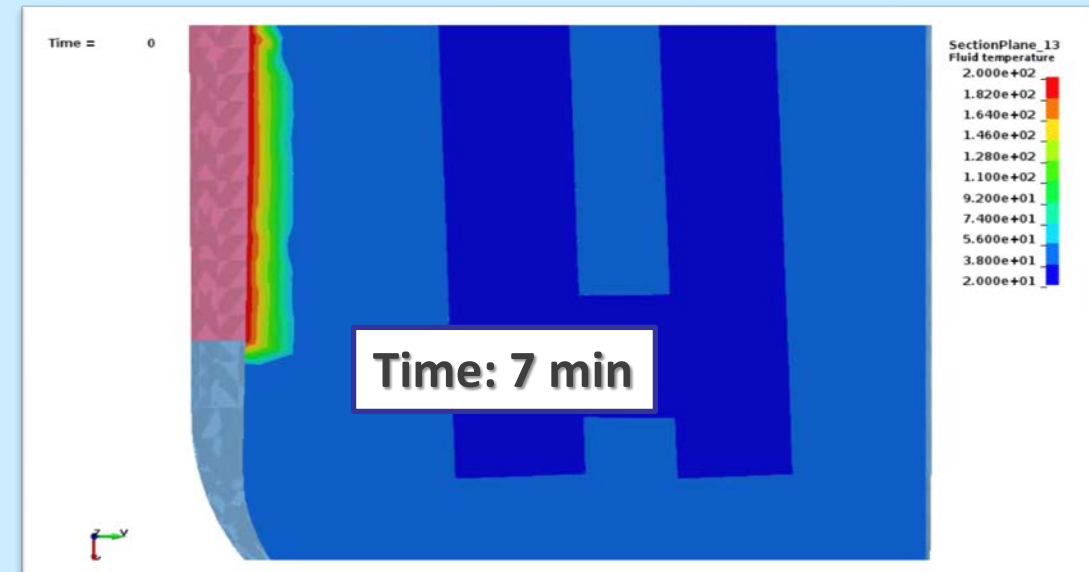
- Conjugate heat solver: Transfer heat from solid to fluid
- Run steady state Navier-Stokes or Potential flow. Use **\*ICFD\_CONTROL\_GENERAL** to set it up.
- Once steady state reached or Potential flow finishes the conjugate heat solver will use the *steady velocity* for the *thermal analysis*.

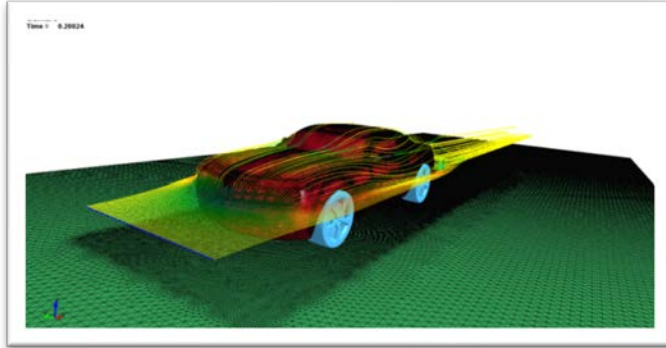


Navier Stokes  
Temperature  
(coupled)



Potential  
Flow  
Temperature

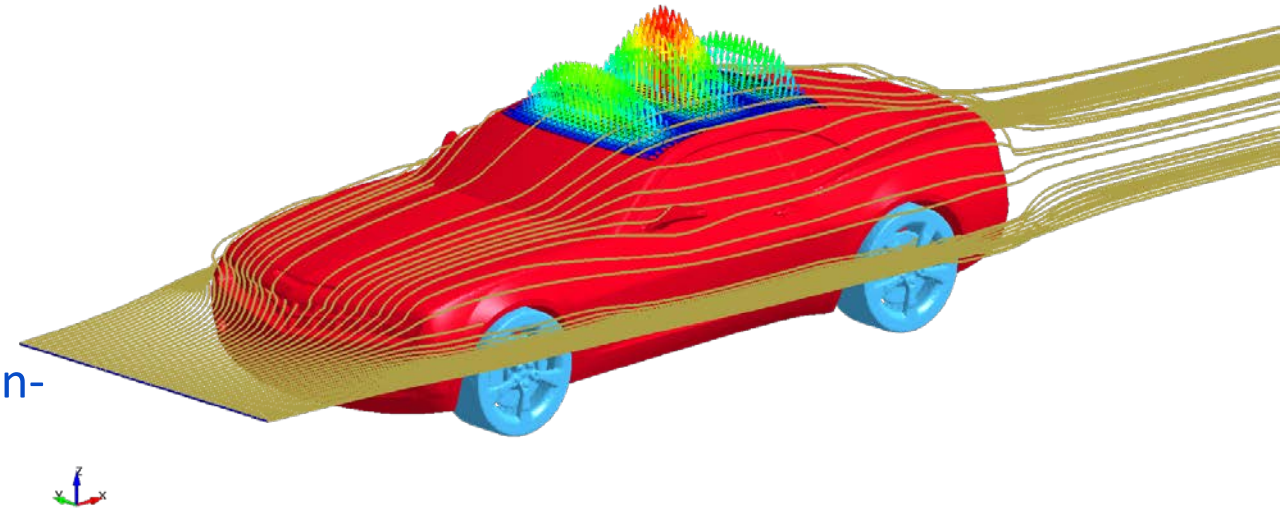
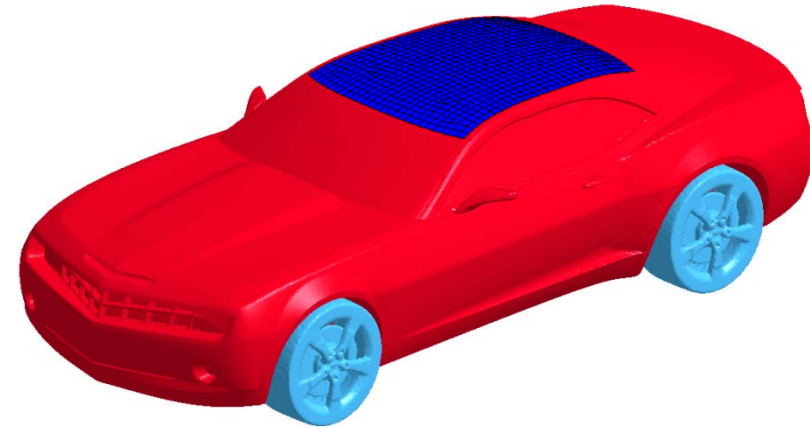




- CFD analysis of full vehicle.
- Couple parts of the structure to analysis the response in a realistic environment.

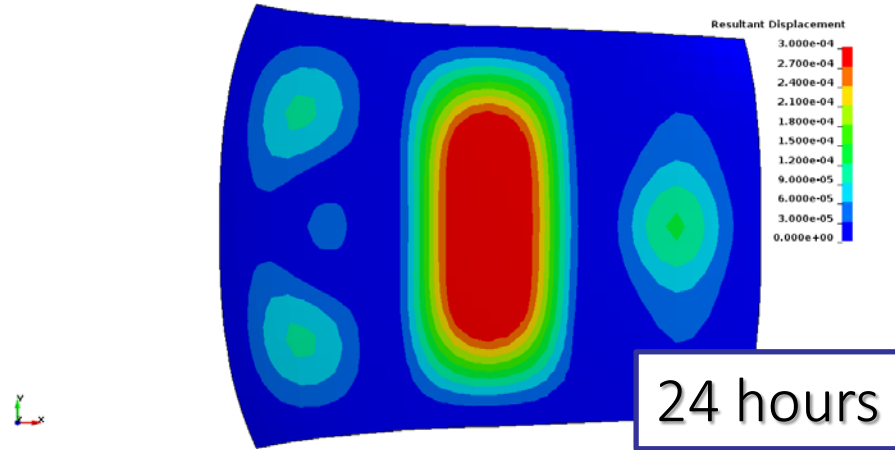
3 different options to solve the same problem:

- Solve **Full Navier–Stokes with FSI** non linear coupling
- Solve **Potential flow**. Provides forces for a non-linear structural analysis
- Solve the **structural analysis alone** using the **output from Navier-Stokes**

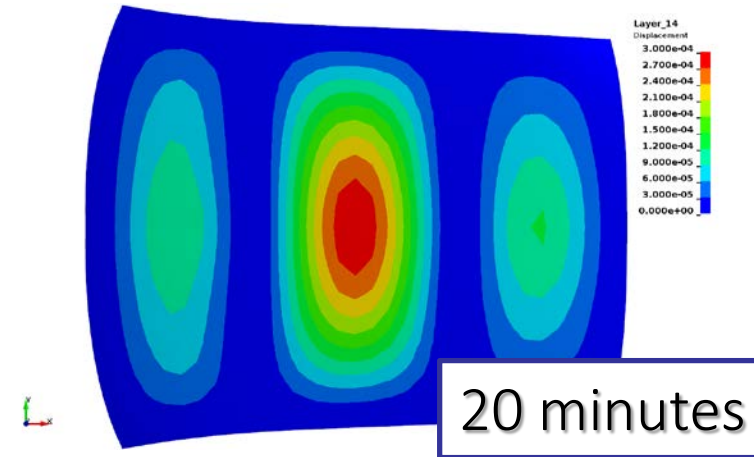




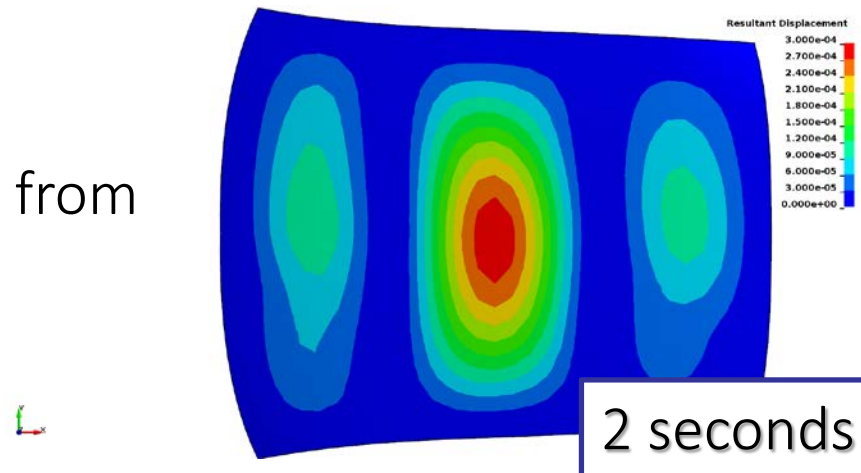
Coupled Navier Stokes

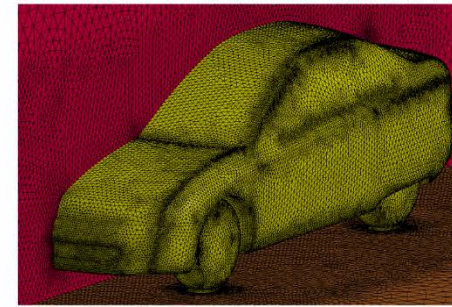
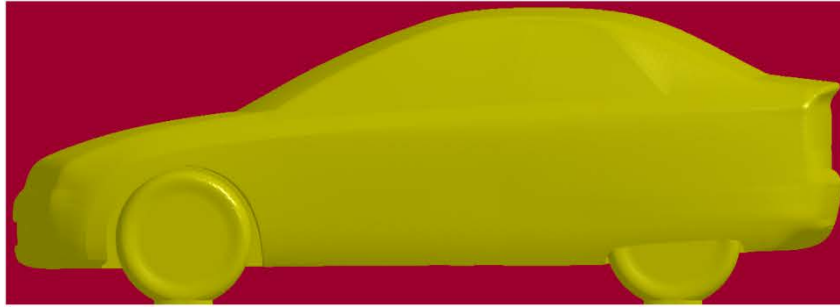


Potential Flow

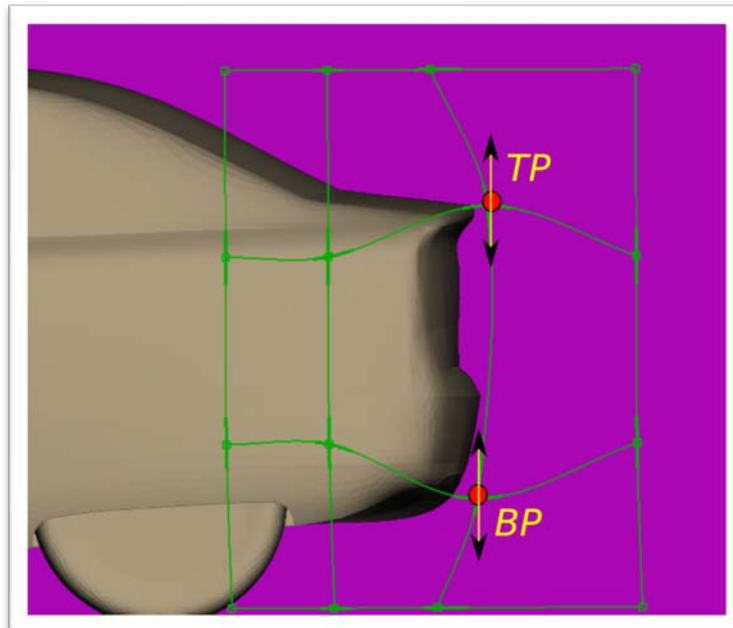


Using \*LOAD\_SEGMENT from  
Navier-Stokes solution

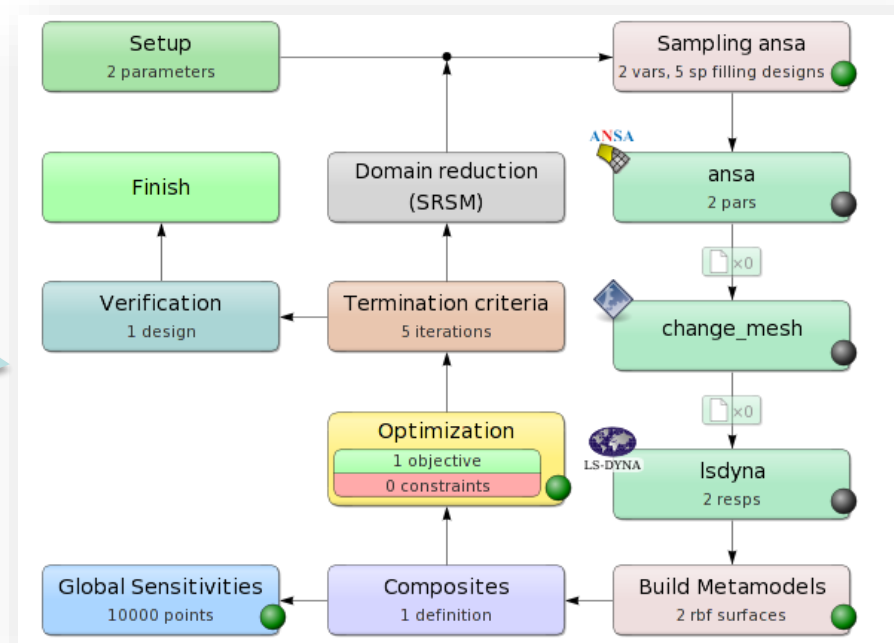




## ANSA morphing



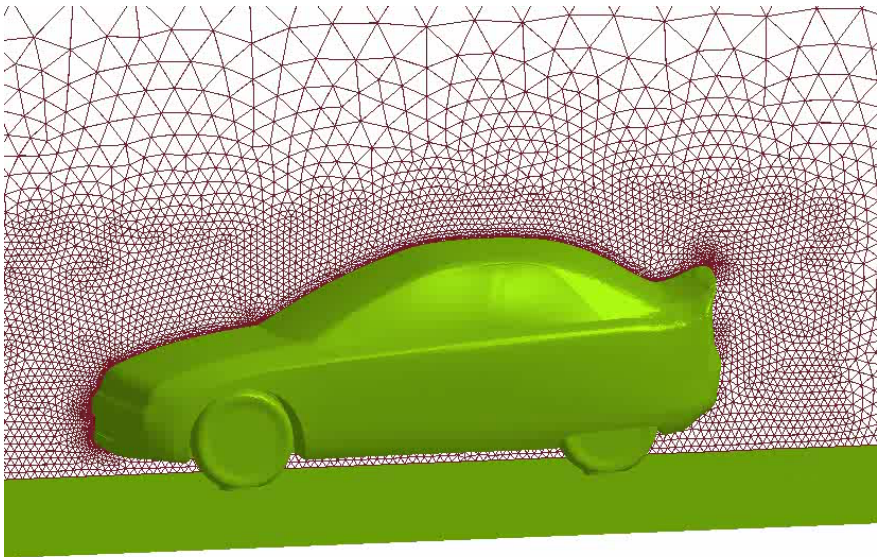
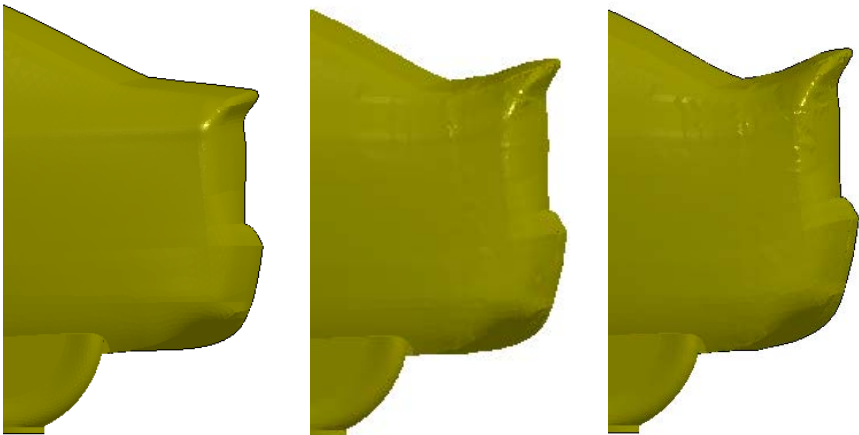
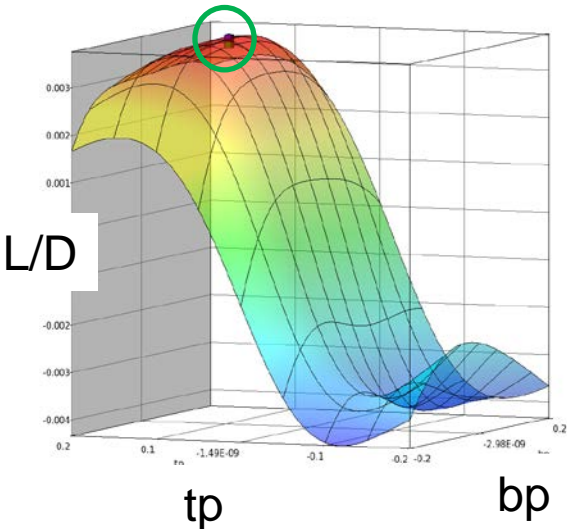
## LS-OPT® Workflow



# Optimal design for (Down Force) / Drag Ratio

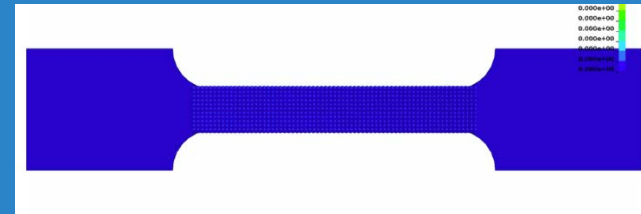
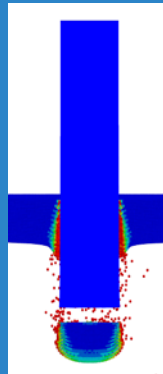
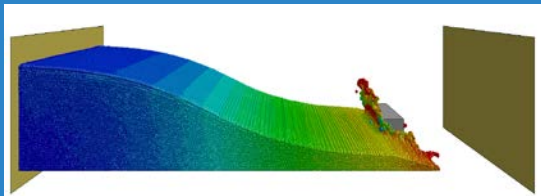
Delpin, Caldichoury, Paz, Wang

| Initial design | Optimal design (6.1) | "Best" design (5.2) |          |
|----------------|----------------------|---------------------|----------|
| 0.0            | 0.022                | 0.062               | bp       |
| 0.0            | 0.105                | 0.132               | tp       |
| -              | 0.00376              | 0.00366             | L/D pred |
| 0.00094        | 0.00364              | 0.00384             | L/D comp |

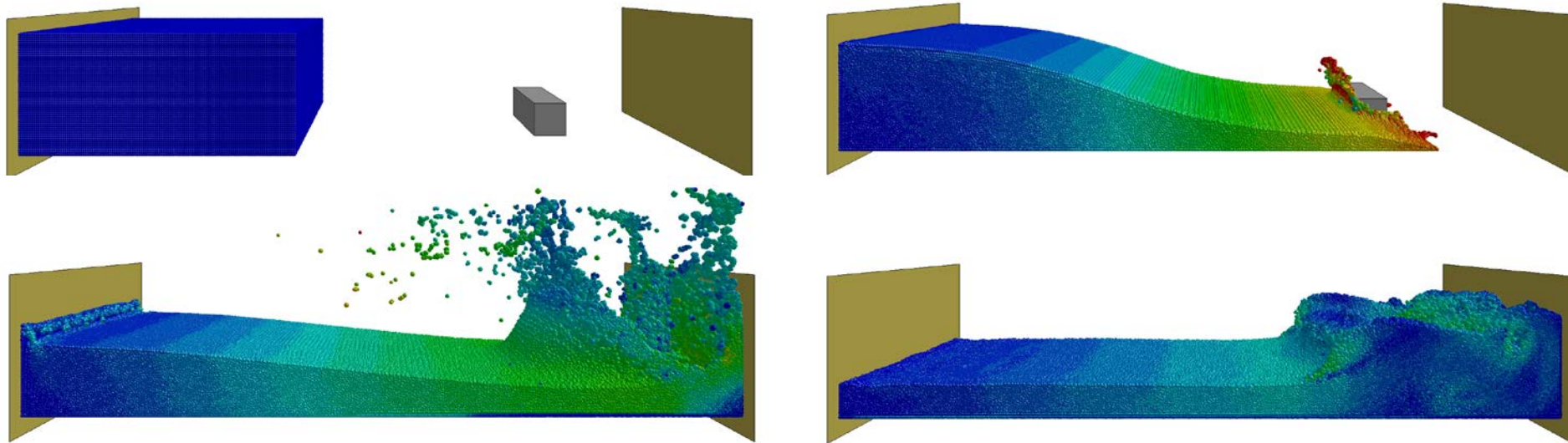


# SPH/CPM Enhancements in LS-DYNA

Dr. Jason Wang  
Dr. Edouard Yreux

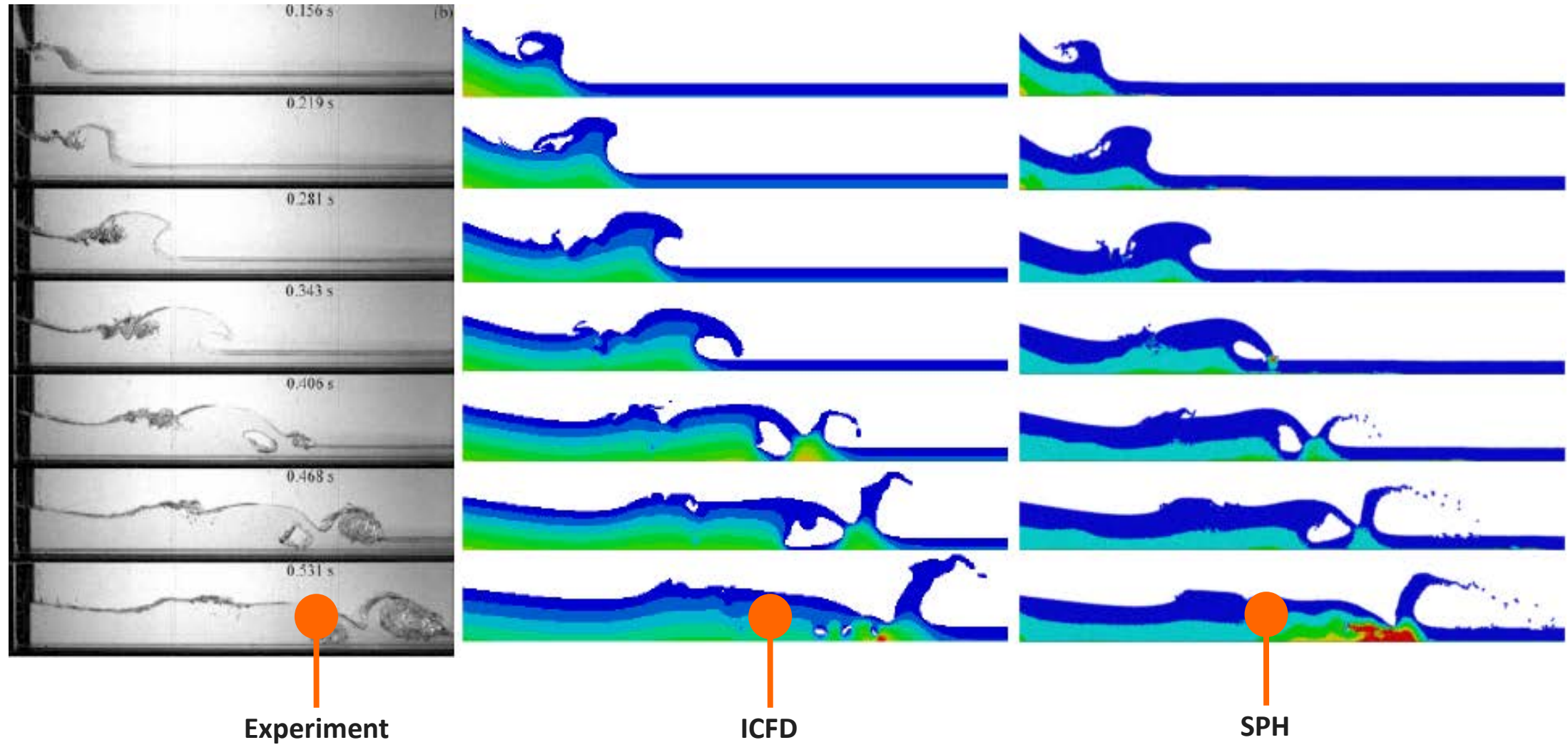


- Density smoothing (to avoid noise) :  $\tilde{\rho}_I = \frac{\sum_J \rho_J \phi_{IJ}}{\sum_J \phi_{IJ}}$  with  $\phi_{IJ} = W_{IJ} m_J / \rho_J$
- Murnaghan Equation of State for weakly compressible modeling (1944)
$$p = k_0 \left[ \left( \frac{\rho}{\rho_0} \right)^\gamma - 1 \right]$$
- Low artificial viscosity is applied for stability

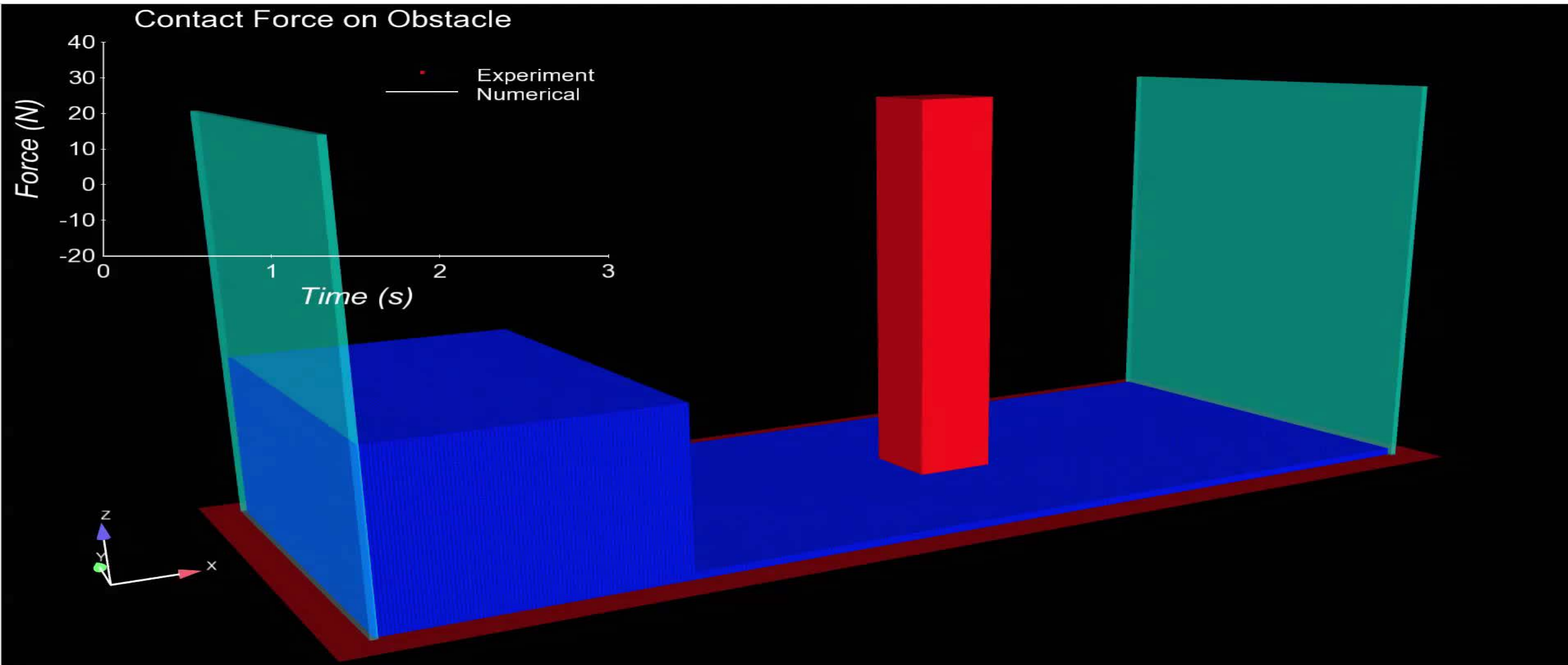


Smooth pressure field - Low compressibility - Reasonable timestep size



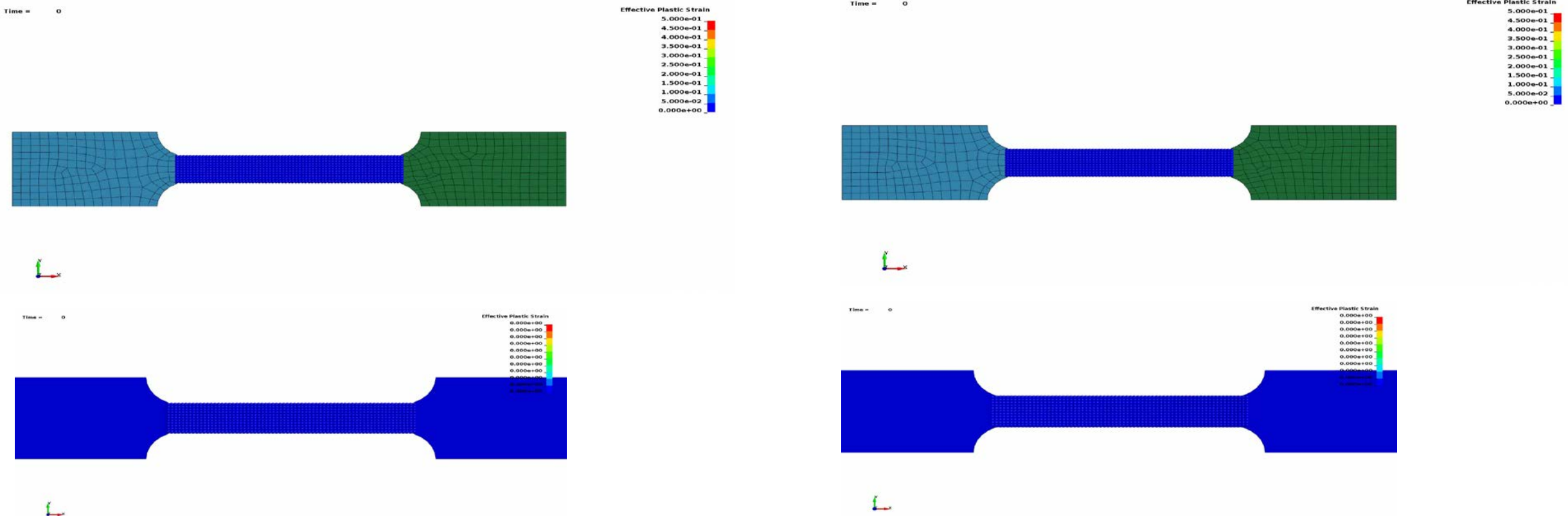


Validated in 2D and 3D formulations





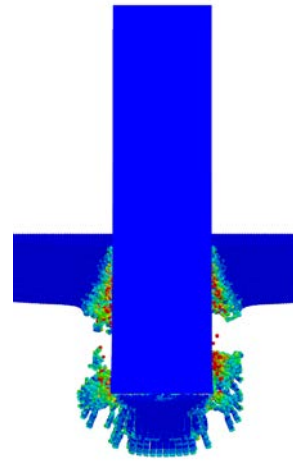
- Quasi-Linear Moving Least-Squares formulation for accuracy and consistency
- Increase support size of the kernel function. Stabilized nodal integration for better stability.
- More CPU-Intensive than regular SPH. A larger support size will increase cost.



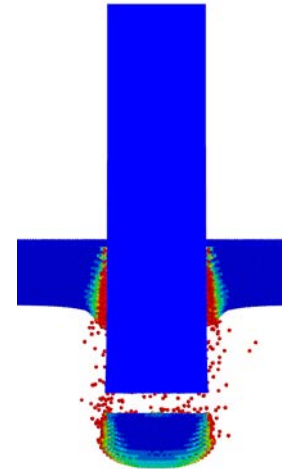
Higher accuracy – Better consistency – Alleviated tensile instability

## Validated for high-velocity impact simulations

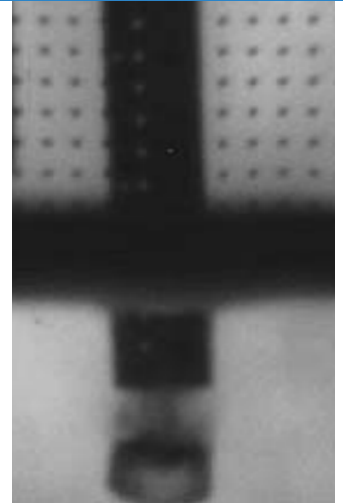
- Quasi-Linear Moving Least-Squares formulation for accuracy and consistency
- Stabilized nodal integration for better stability
- More CPU-Intensive than regular SPH



Traditional SPH



MLS-Based SPH



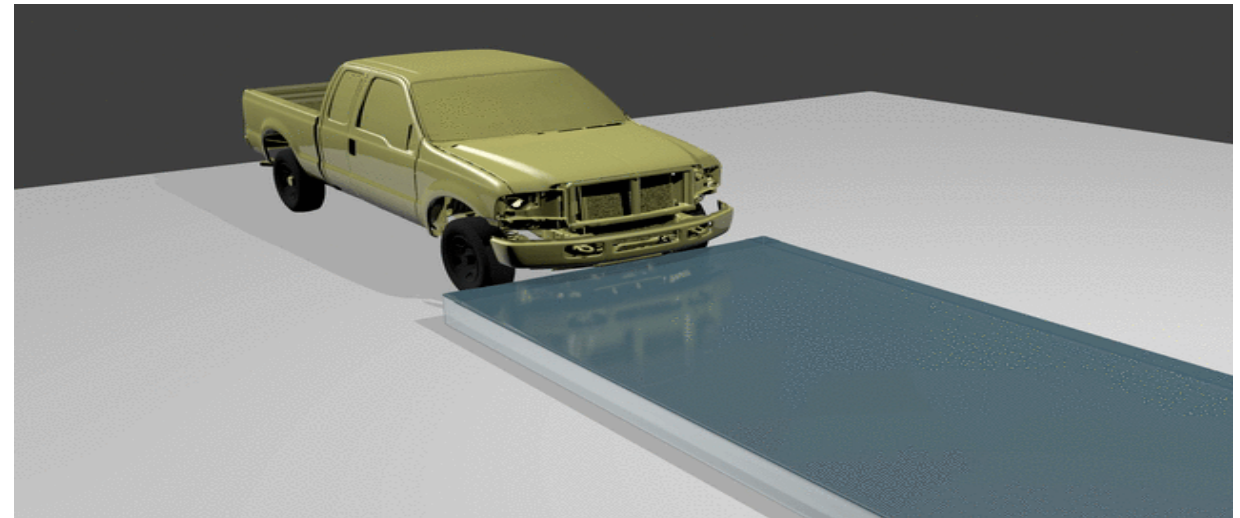
Experiment

| Comparison With Experimental Data |              |           |       |           |       |
|-----------------------------------|--------------|-----------|-------|-----------|-------|
|                                   | Experimental | Form 0    |       | Form 12   |       |
| Projectile Residual Velocity      | 199.7 m/s    | 207.9 m/s | 3.9%  | 201.6 m/s | 0.9%  |
| Plug Residual Velocity            | 242.3 m/s    | 212 m/s   | 12.5% | 248 m/s   | 2.4%  |
| Plug Mass                         | 27.6 g       | 35.9 g    | 23.1% | 28.9 g    | 4.7%  |
| Plug Height                       | 11.4 mm      | 17.6 mm   | 54.4% | 11.3 mm   | 0.9%  |
| Crater, front diameter            | 20.7 mm      | 20.4 mm   | 1.4%  | 20.6 mm   | 0.5%  |
| Crater, exit diameter             | 20.9 mm      | 30.8 mm   | 47.4% | 23.7 mm   | 13.4% |

- Implicit, incompressible SPH formulation allows larger timestep size
- Tailored for wading-type problems
- Example with 9.1 million particles:

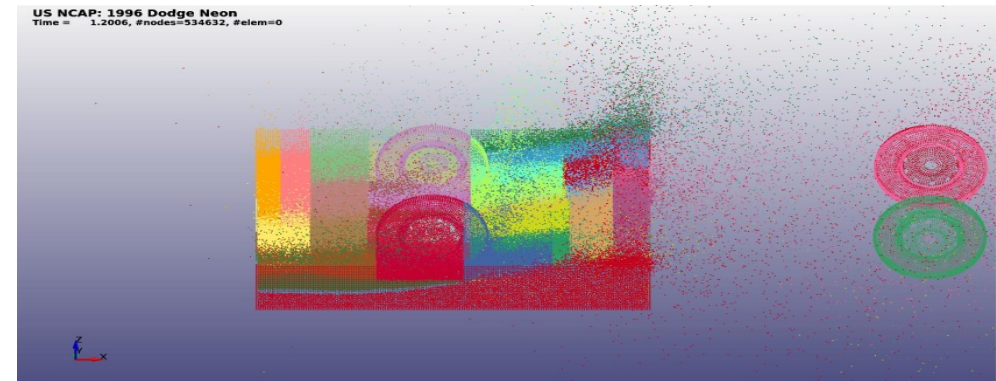
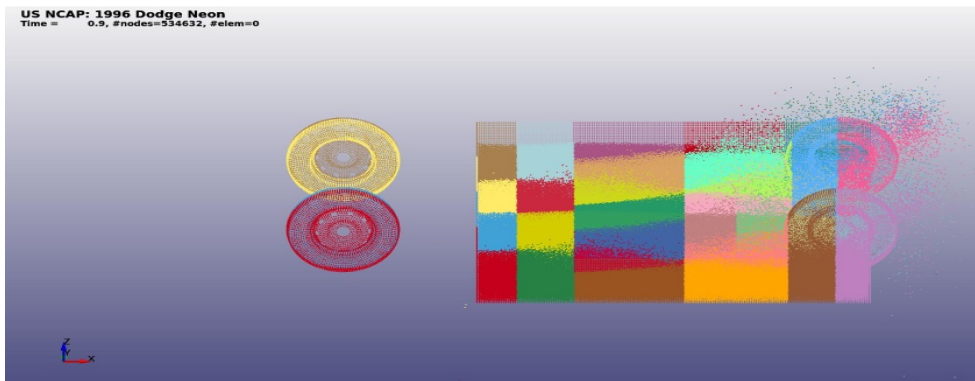
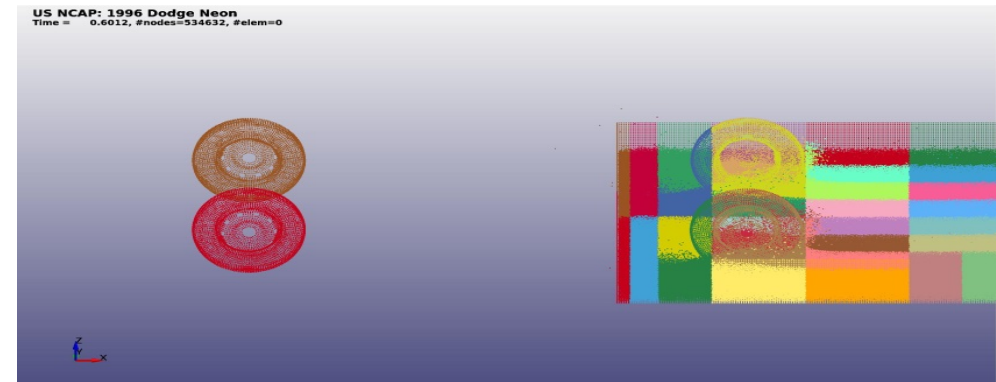
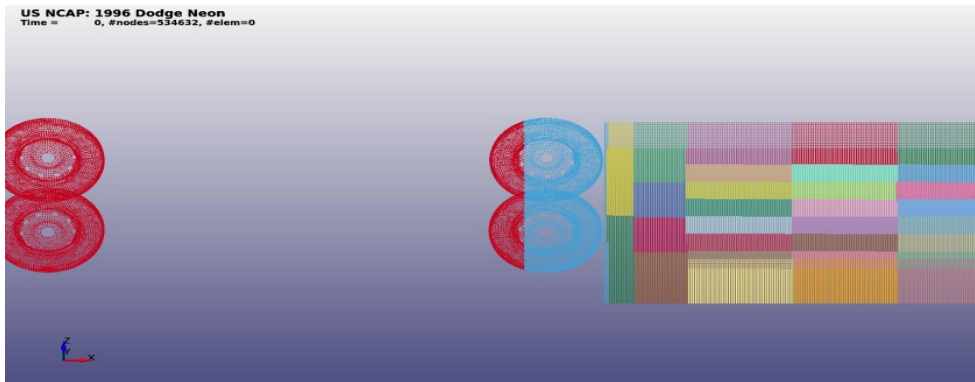


**Implicit SPH**  
**Color-coded by velocity**



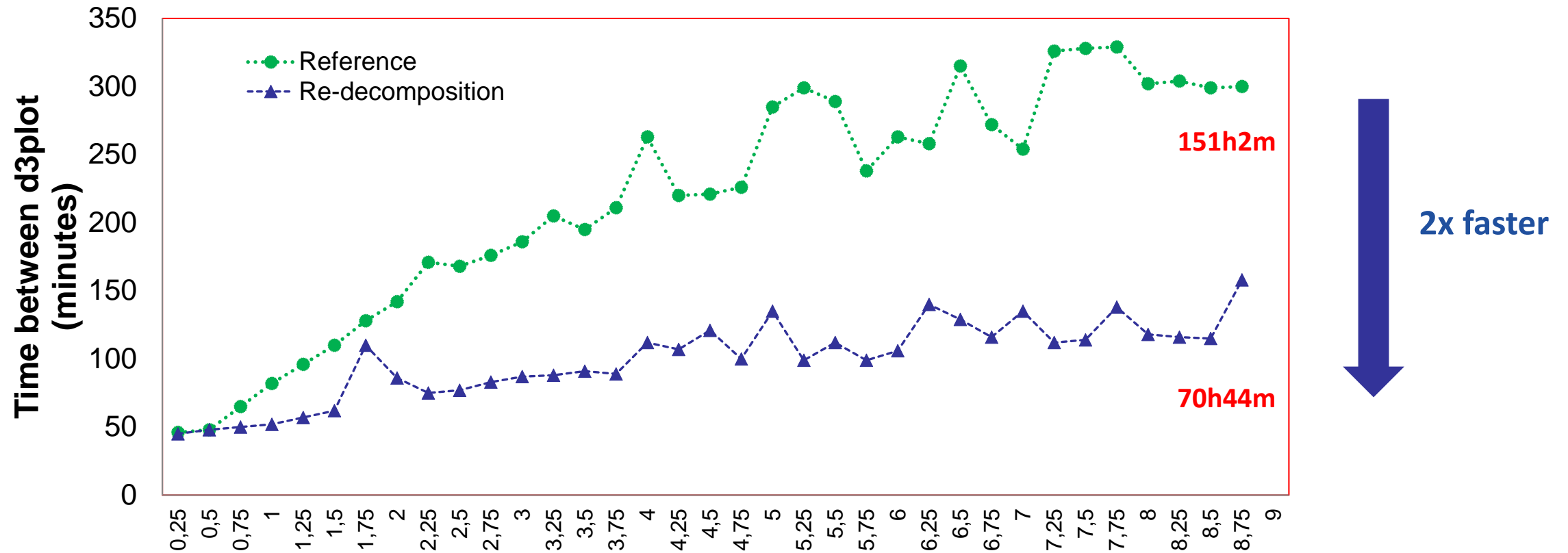
**Blender rendering**

- Large deformation can cause load unbalancing among processors
- Re-decomposed the model several times during simulation using a fulldeck restart
- `decomp { defgeo }` : The model is decomposed using the current deformed geometry



# Re-decomposition

Wang, Yreux



- More development work to make an automated process similar to adaptive simulation.
- Currently it uses fulldeck restart capability, user has full control to get better performance.
- Testing other problems, i.e. bird strike, small offset, ODB, etc.

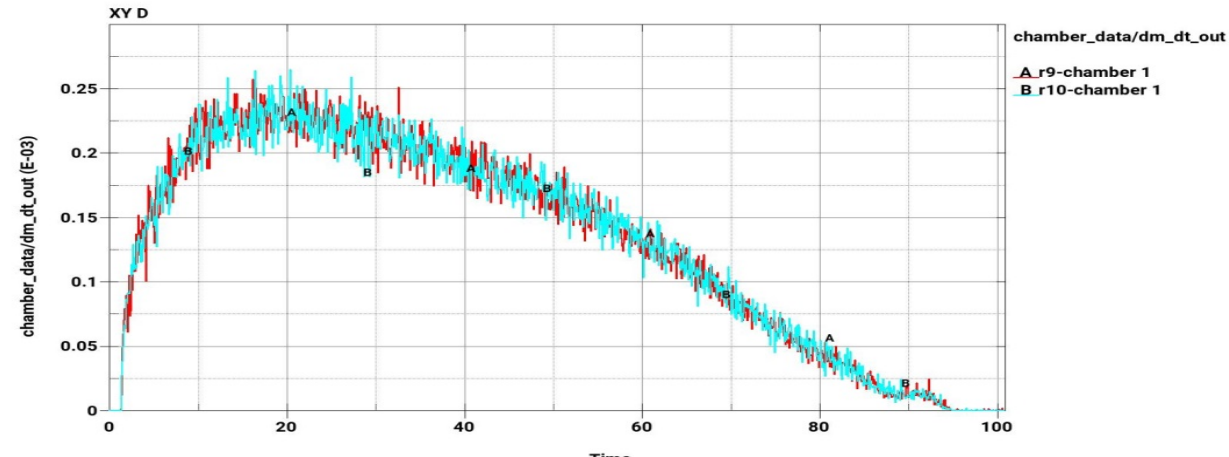
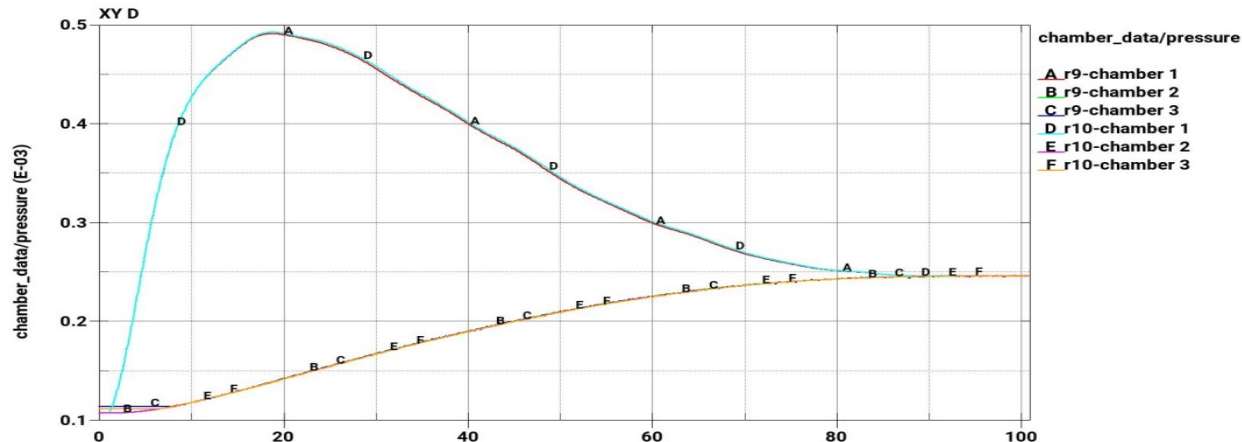
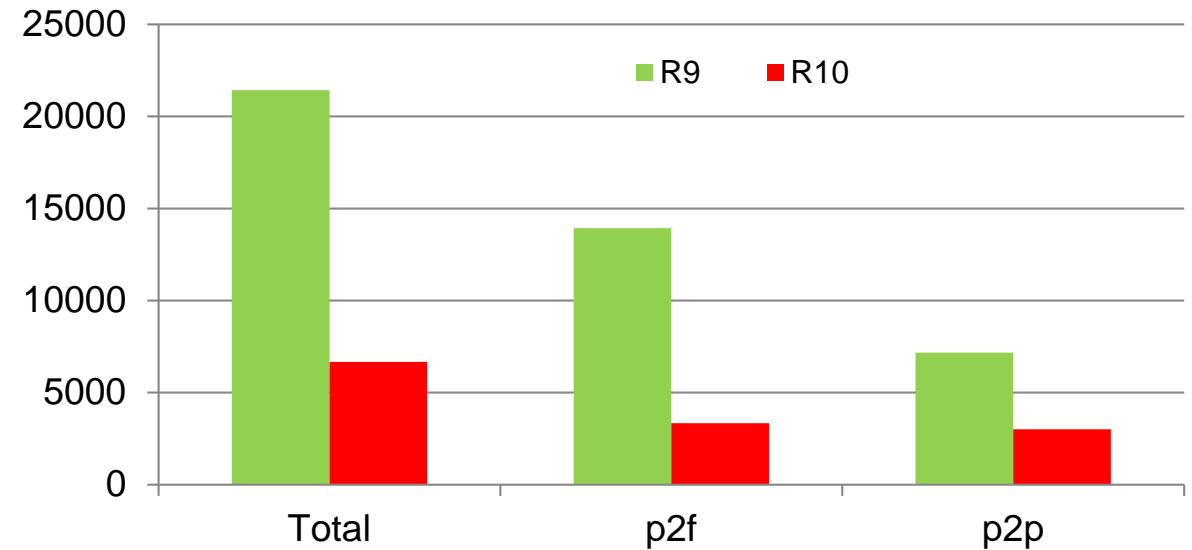


# CPM | New CPM for AIRBAG Simulations

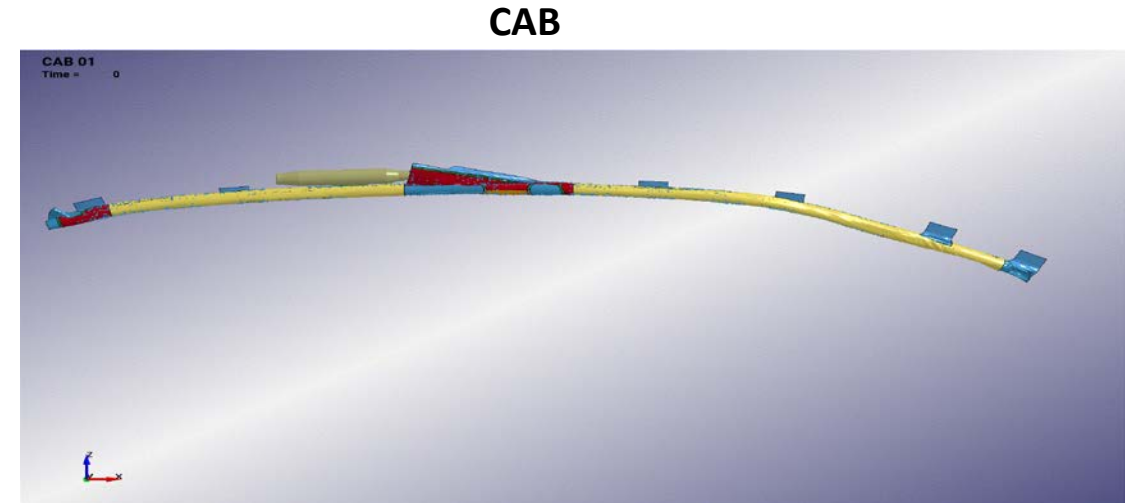
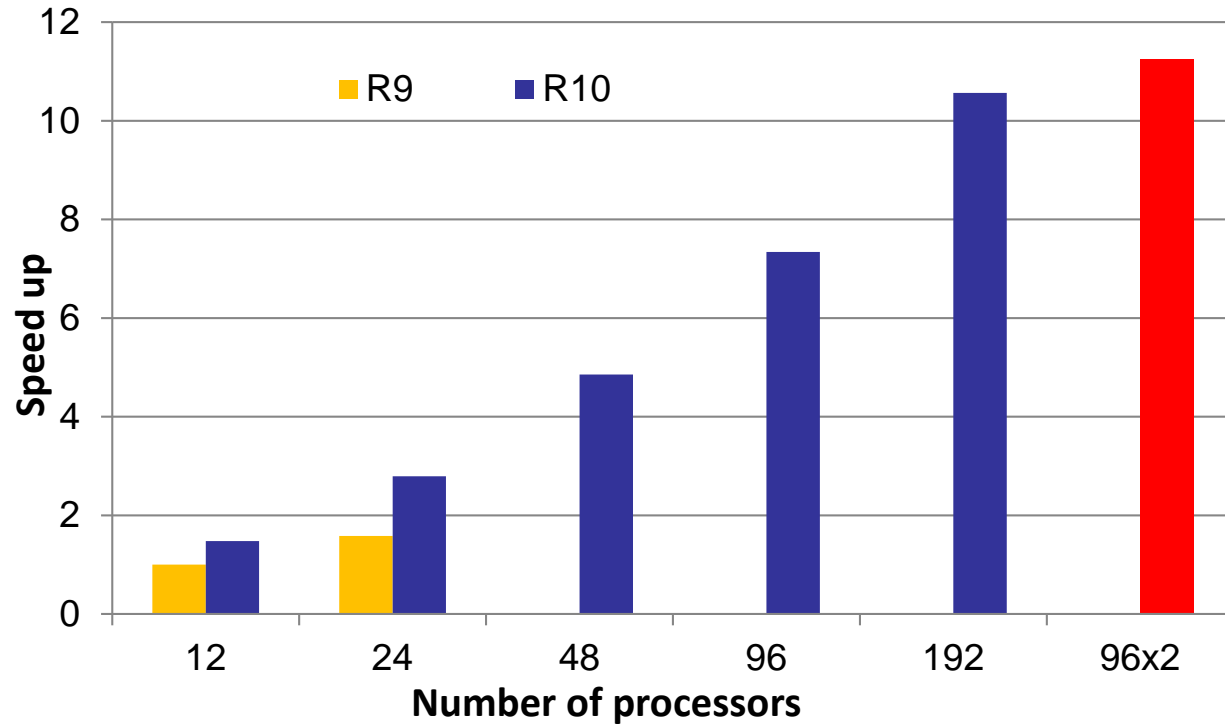
- Main cost for airbag simulation, (1)airbag self contact, (2)p2f and (3)p2p
- New and faster particle to fabric (p2f) contact algorithm
- Redistribute CPM particles among processors to achieve better scaling and efficient particle to particle (p2p) collisions

- **Speedup: 3x for tank test**
- **Validation: Pressure history is consistent between releases**

Elapsed time (seconds)



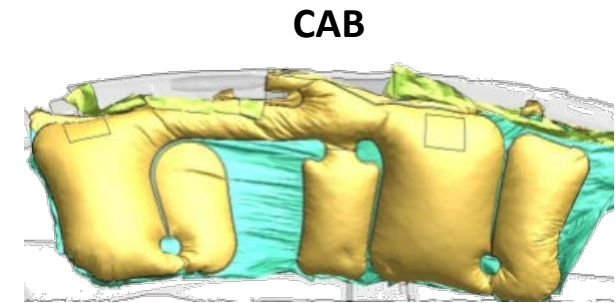
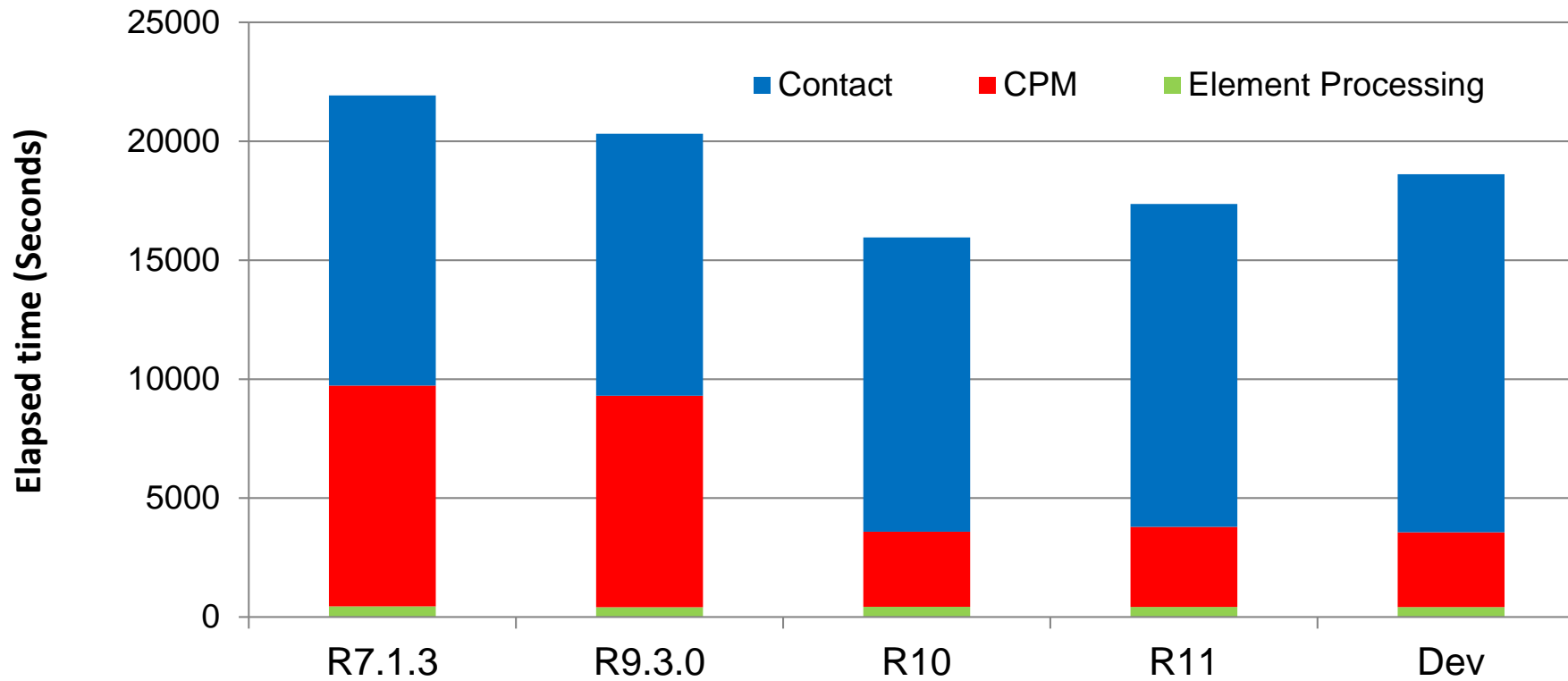
# CPM | CAB Performance Improvement



- OpenMP (HYBRID) enabled as the default algorithm. See 96x2 (red bar)
- Reduced amount of data transferring between processors for better scaling
- It is more efficient for the full vehicle simulation which uses more than 200 processors
- Same input faster turn around time (no additional user input)



# Special decomposition



- Performance was measured with 96 processors
- CPM is about 3x faster from R7 to R10
- Self contact about the same
- The overall speed up is about 20%.

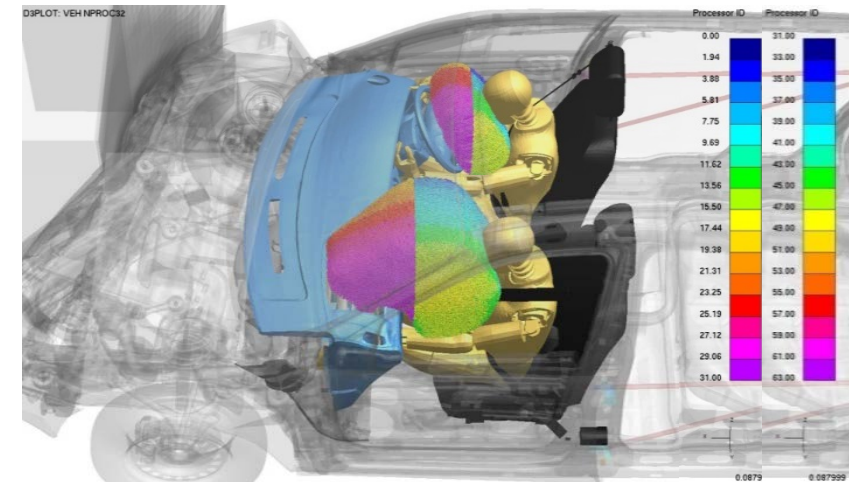
# Special decomposition: airbag-dedicated processor group

\*CONTROL\_MPP\_DECOMPOSITION\_ARRANGE\_PARTS

*Part/Part Set ID, TYPE, NPROC, FRSTP*

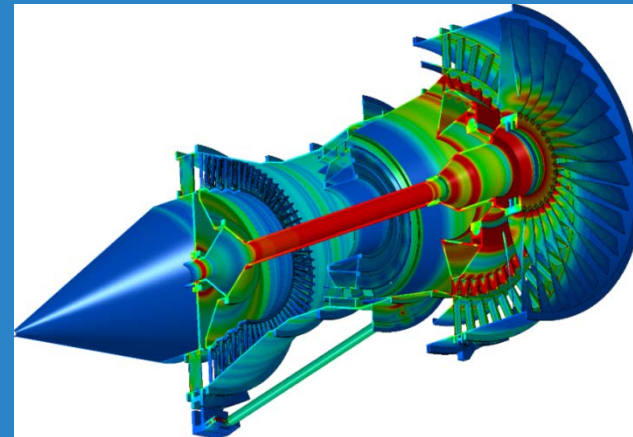
*pfile options: region { parts/partset ID NPROC FRSTP }*

- New decomposition allows distributing workload into user defined processors group.
- Multiple CPM airbags can be arranged into subset of processors.
- Each CPM airbag and its self contact runs independently to achieve best parallel efficiency.



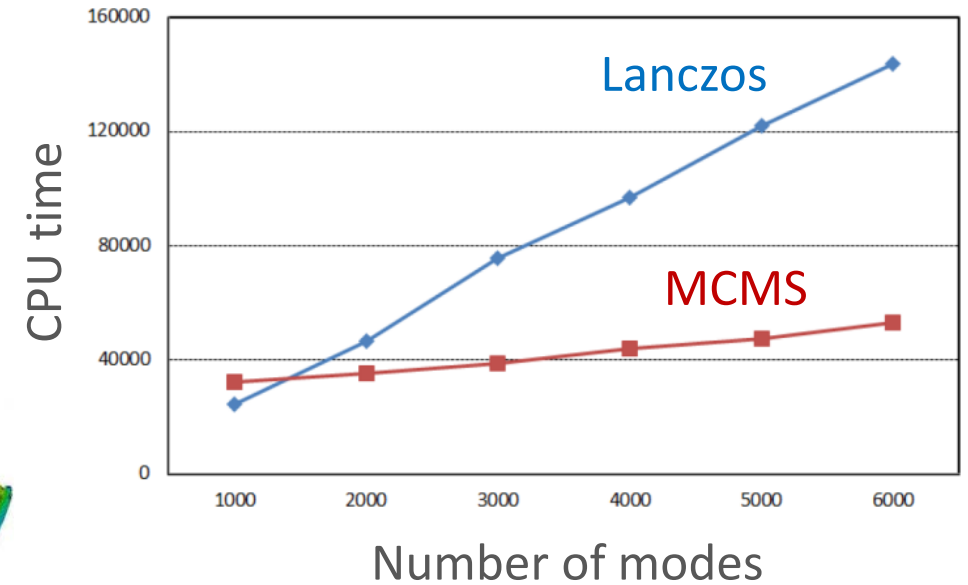
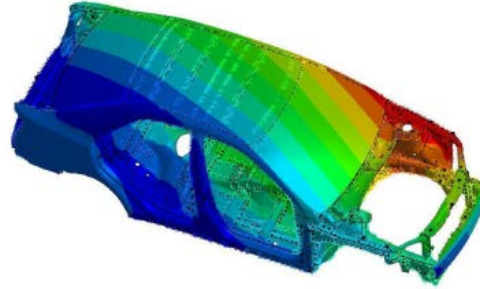
# Linear Implicit Analysis

Grimes, Ashcraft, Lucas, Rouet, Wiesbecker, Vecharynski, Li



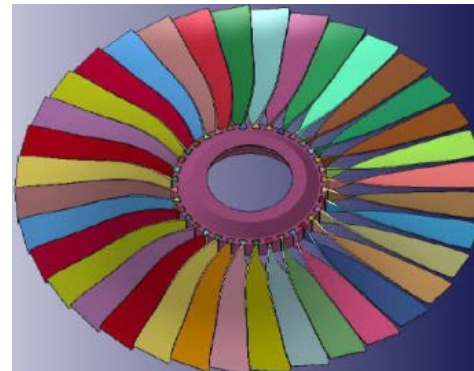
- New eigenvalue extraction method: MCMS

- Multilevel Component Mode Synthesis
- Based on multilevel substructuring (AMLS)
- less accurate than Lanczos, but far less computer resources
- useful for NVH applications that want thousands of modes



- Sectoral symmetry

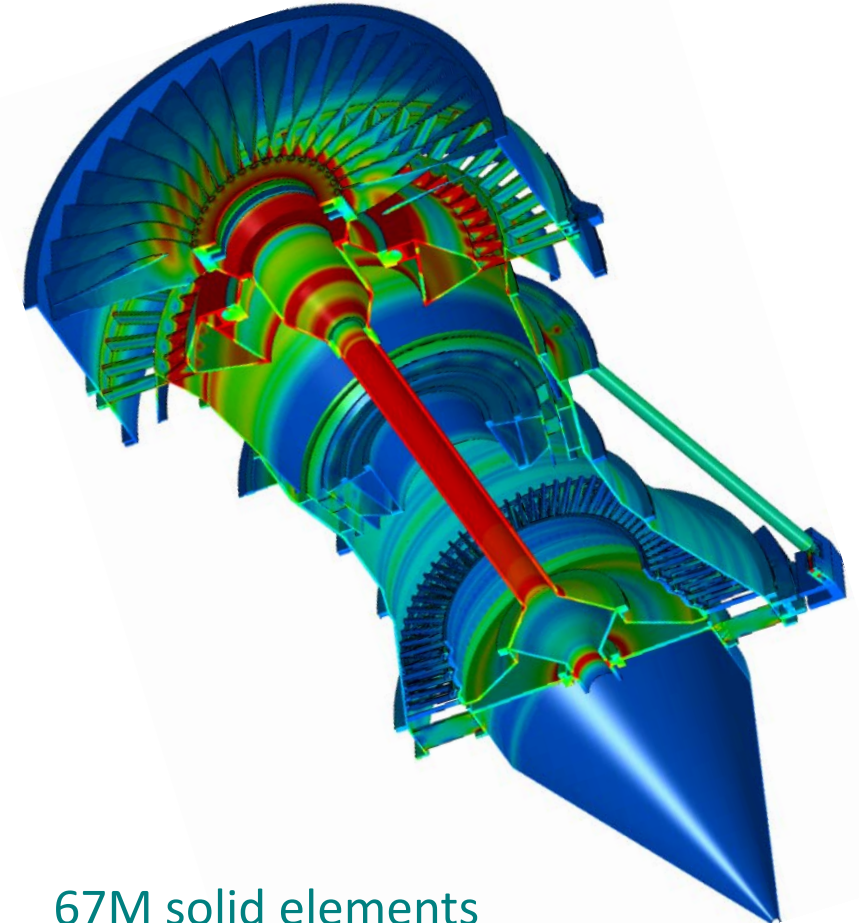
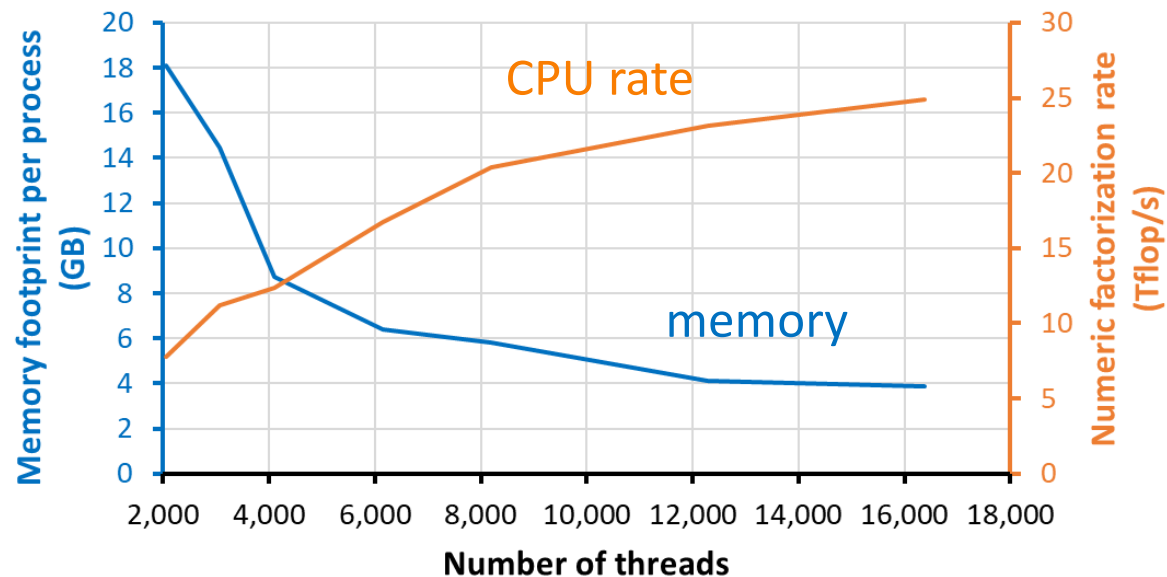
- 1,000,000 elements per blade
- for models with significant rotational symmetry: highly reduced eigenvalue problem



huge CPU/memory savings

- And always...

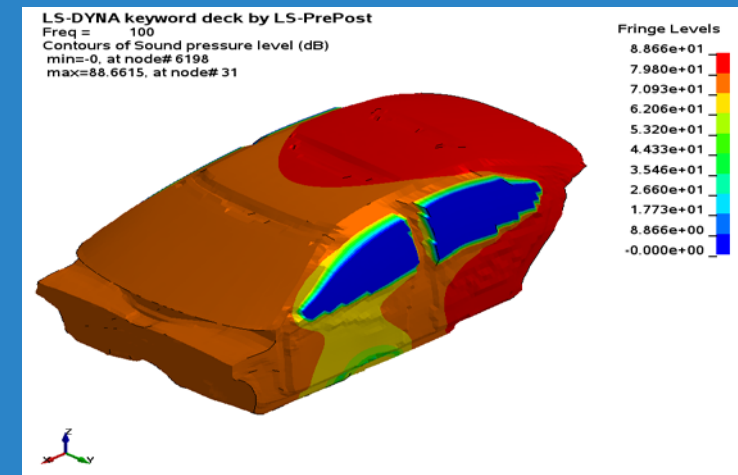
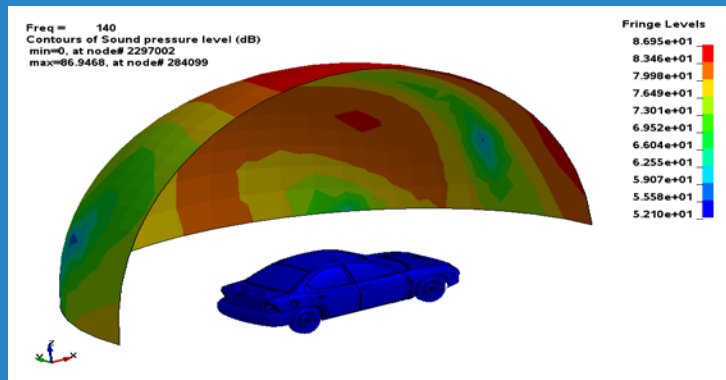
- ...working on larger and larger models!
  - e.g. static loading of jet engine model from Rolls-Royce
  - original attempt: 158 hours on 448 cores
  - current best: 12 hours on 2304 cores
  - continuing efforts to improve scalability
  - Eigenvalue problem not analyzed yet



67M solid elements  
200M rows in linear system

# Acoustic and Fatigue Analysis

Dr. Yun Huang





## Vibration solvers

- Frequency Response Function
- Steady State Dynamics
- Random Vibration
- Response Spectrum Analysis

## Fatigue solvers

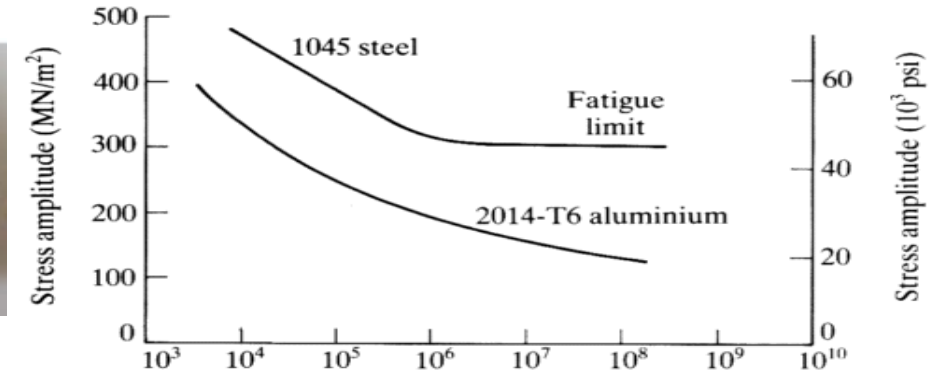
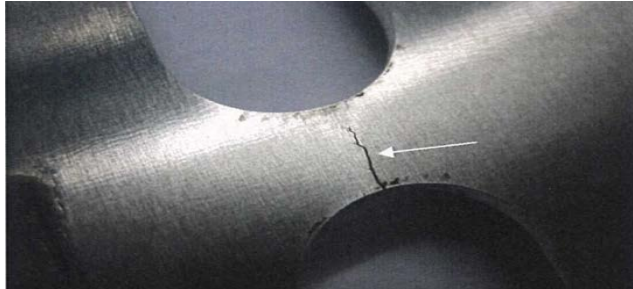
- Random Vibration Fatigue (Frequency)
- SSD fatigue (Frequency)
- Time domain fatigue
  - Stress based
  - Strain based

## Acoustic solvers

- Boundary Element Method
  - Collocation
  - Indirect
  - Rayleigh Method
  - Kirchhoff Method
- Finite Element Method
- Acoustic Eigenvalue Analysis
- Statistical Energy Analysis

## Applications

- NVH analysis of automotive and aerospace
- Civil and hydraulic Engineering
- Earthquake engineering
- Acoustic simulation
- Fatigue and durability

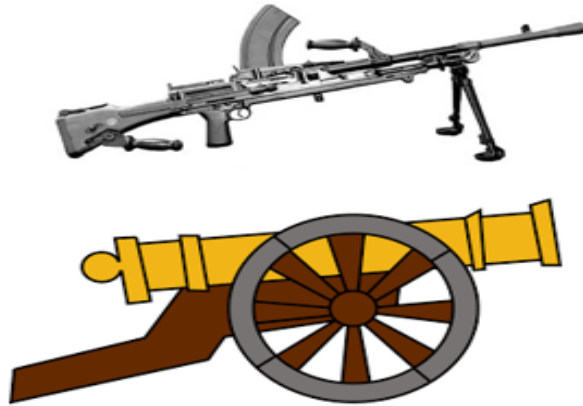


- Frequency domain fatigue solvers
  - random vibration environment
  - SSD environment
- Advantages
  - Integration of vibration and fatigue solver in one code
  - A wide selection of stress / strain solvers in LS-DYNA (implicit, explicit, etc.)
  - Manufacturing effects (e.g. residual stress in metal forming) can be considered
  - User chooses to run fatigue analysis on whole model, part, set of parts, or set of elements of interest.
  - Future integration with LS-OPT / LS-TaSC for multidisciplinary optimization
- Time domain fatigue solvers
  - based on stress (*high cycle, low stress*)
  - based on strain (*plastic deformation*)

# Time domain fatigue – Stress based example

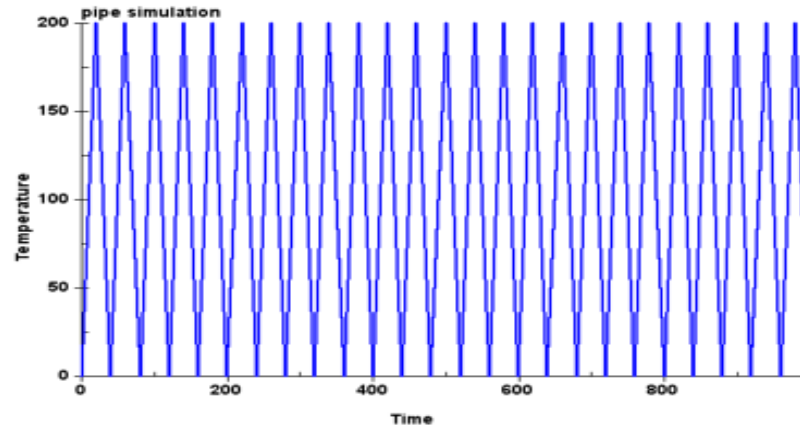
Huang

*This example studies the fatigue life of a metal tube, under cyclic thermal stress condition, which is caused by gunfire or other events which are characterized by cyclic temperature change*



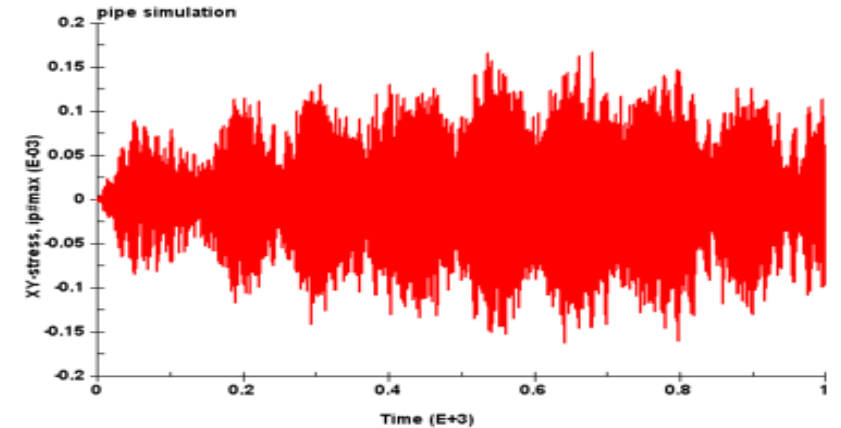
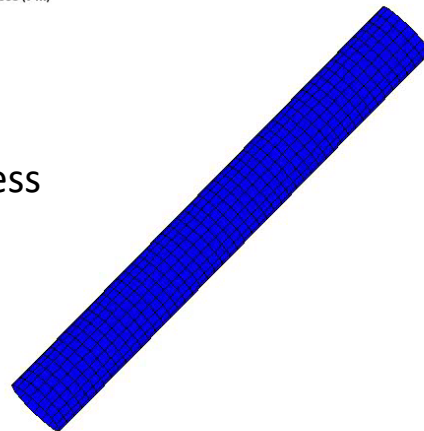
pipe simulation  
Time = 0  
Contours of Effective Stress (v-m)  
max IP. value  
min=0, at elem# 1000  
max=0, at elem# 1000

Effective stress



Effective Stress (v-m)

0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00  
0.000e+00

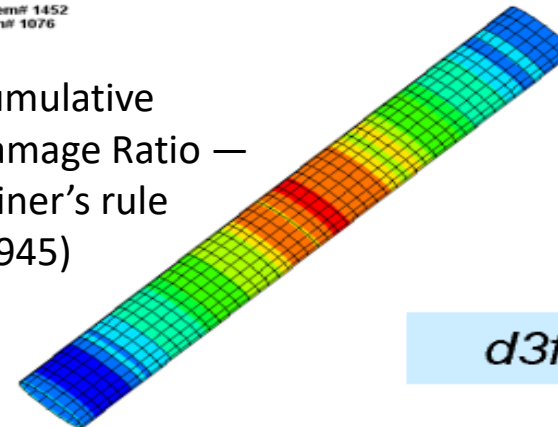


pipe simulation  
Contours of Cumulative damage ratio  
max IP. value  
min=0.000231687, at elem# 1452  
max=0.0028434, at elem# 1076

Cumulative  
Damage Ratio —  
Miner's rule  
(1945)

Cumulative damage ratio

2.843e-03  
2.582e-03  
2.321e-03  
2.060e-03  
1.799e-03  
1.538e-03  
1.276e-03  
1.015e-03  
7.540e-04  
4.929e-04  
2.317e-04



d3ftg

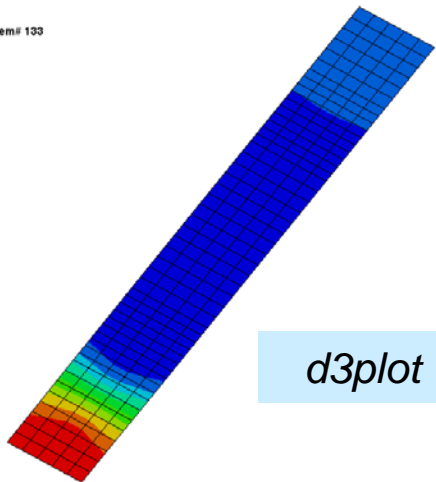
# Initial Fatigue Damage Ratio

Accumulate damage using previous damage due to loading or fatigue

- Defined by `*INITIAL_FATIGUE_DAMAGE_RATIO`
  - Initial damage ratio (e.g. Miners's rule) can come from *past fatigue* analysis (d3ftg)
  - Initial damage ratio can come from *transient preload* (d3plot), e.g. `*mat_add_erosion`, `*mat_add_damage_gissmo`, etc.
- Summed up by `*FATIGUE_SUMMATION`

Time = 0.030006  
Contours of History Variable#1  
max IP. value  
min=0, at elem# 33  
max=0.147016, at elem# 133

History Variable#1  
1.470e-01  
1.323e-01  
1.176e-01  
1.029e-01  
8.821e-02  
7.351e-02  
5.881e-02  
4.410e-02  
2.940e-02  
1.470e-02  
0.000e+00

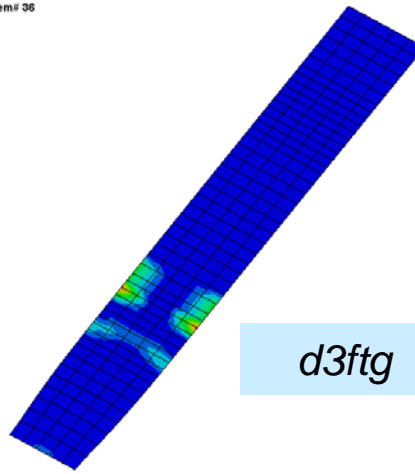


d3plot

Damage from transient preload case (d3plot)

Contours of Cumulative damage ratio  
max IP. value  
min=0.00190821, at elem# 106  
max=0.344004, at elem# 36

Cumulative damage ratio  
3.440e-01  
3.098e-01  
2.756e-01  
2.414e-01  
2.072e-01  
1.730e-01  
1.387e-01  
1.045e-01  
7.033e-02  
3.612e-02  
1.908e-03

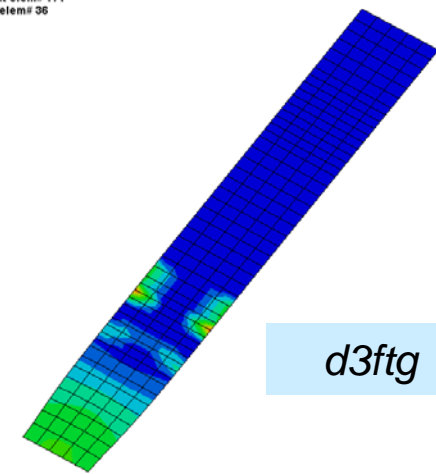


d3ftg

Damage ratio from fatigue load

Contours of Cumulative damage ratio  
max IP. value  
min=0.00253502, at elem# 171  
max=0.344281, at elem# 36

Cumulative damage ratio  
3.443e-01  
3.101e-01  
2.759e-01  
2.418e-01  
2.076e-01  
1.734e-01  
1.392e-01  
1.051e-01  
7.089e-02  
3.671e-02  
2.539e-03



d3ftg

Cumulative damage ratio from transient preload + fatigue load

# Multi-axial fatigue analysis

Stress / strain state is always three dimensional (two-dimensional on surface): *scalarize* the problem, using ...

- A scalar index (e.g. von-mises stress, 1<sup>st</sup> principal stress) can be used
- Fatigue damage is computed on multiple planes and the max value is picked
- A critical plane is located and fatigue analysis is performed on the critical plane

```
*FATIGUE_ELOUT
$#      ssid      sstype
$#      dt
$#      stres      index
$#      stres      index      1

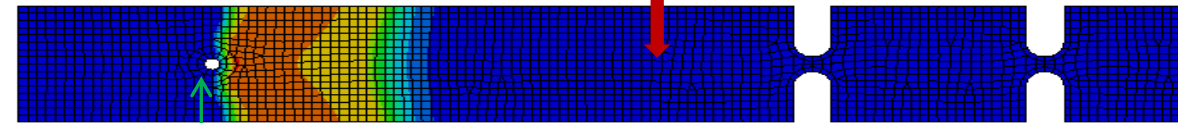
*FATIGUE_MULTIAXIAL
$#      maxial      nplane
$#      1          180
```

| maxial | nplane | Max damage ratio |
|--------|--------|------------------|
| 0      |        | 1.26547          |
| 1      | 18     | 1.30282          |
| 1      | 36     | 1.30282          |
| 1      | 72     | 1.30327          |
| 1      | 180    | 1.30327          |
| 2      |        | 1.30445          |

Time = 10000  
Contours of Cumulative damage ratio  
max IP. value  
min=0, at elem# 5462  
max=1.26547, at elem# 5291

$$F(t) = \sin(22\pi \cdot t)$$

maxial=0



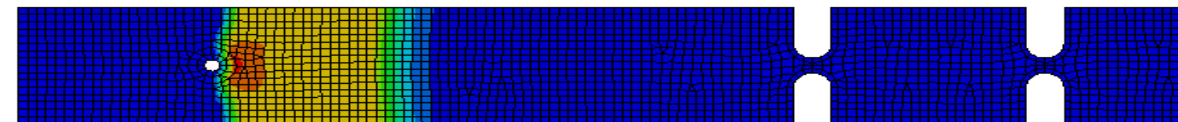
Cumulative damage ratio

|           |
|-----------|
| 1.265e+00 |
| 1.139e+00 |
| 1.012e+00 |
| 8.858e-01 |
| 7.593e-01 |
| 6.327e-01 |
| 5.062e-01 |
| 3.796e-01 |
| 2.531e-01 |
| 1.265e-01 |
| 0.000e+00 |

Time = 10000  
Contours of Cumulative damage ratio  
max IP. value  
min=0, at elem# 5462  
max=1.30445, at elem# 5291

d3ftg

maxial=2

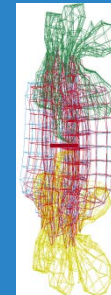
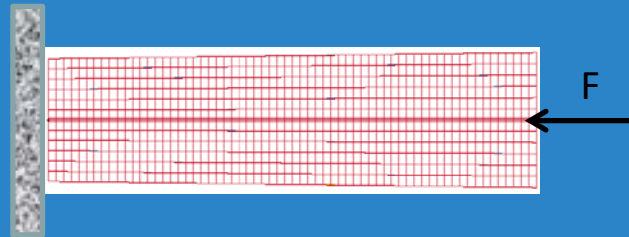


Cumulative damage ratio

|           |
|-----------|
| 1.304e+00 |
| 1.174e+00 |
| 1.044e+00 |
| 9.131e-01 |
| 7.827e-01 |
| 6.522e-01 |
| 5.218e-01 |
| 3.913e-01 |
| 2.609e-01 |
| 1.304e-01 |
| 0.000e+00 |

# Crushable Nonlinear Beam

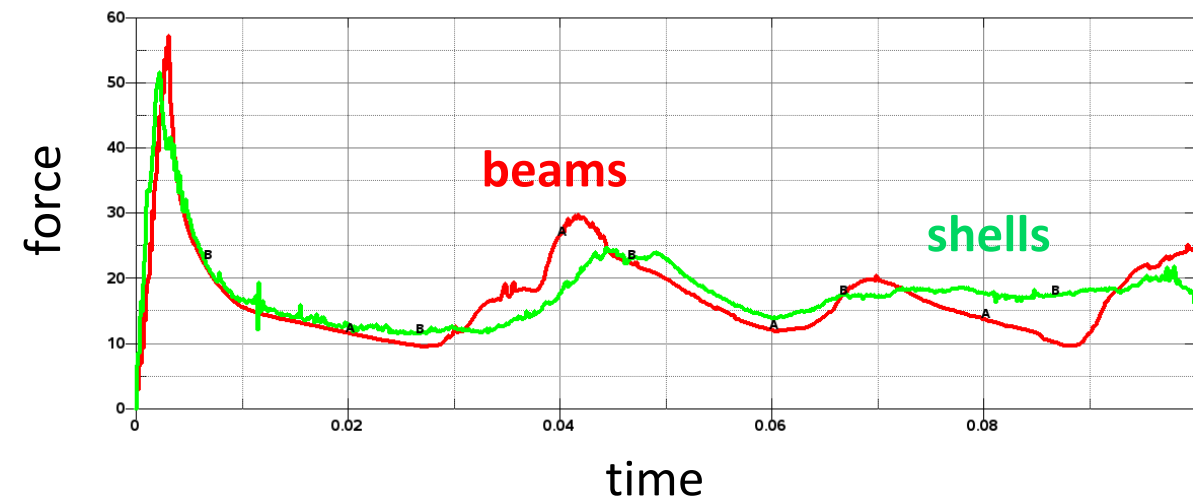
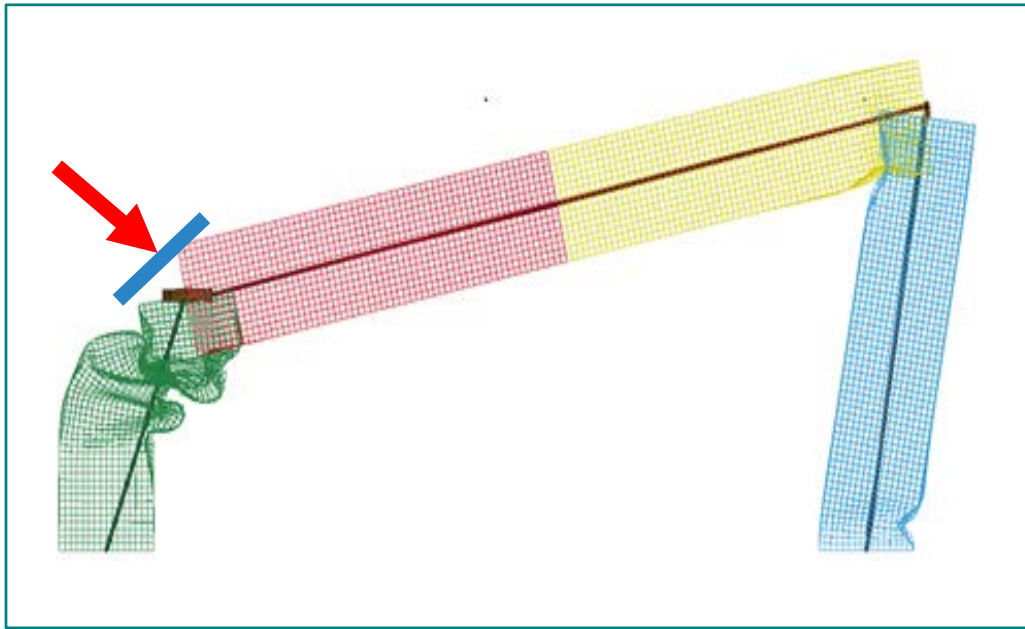
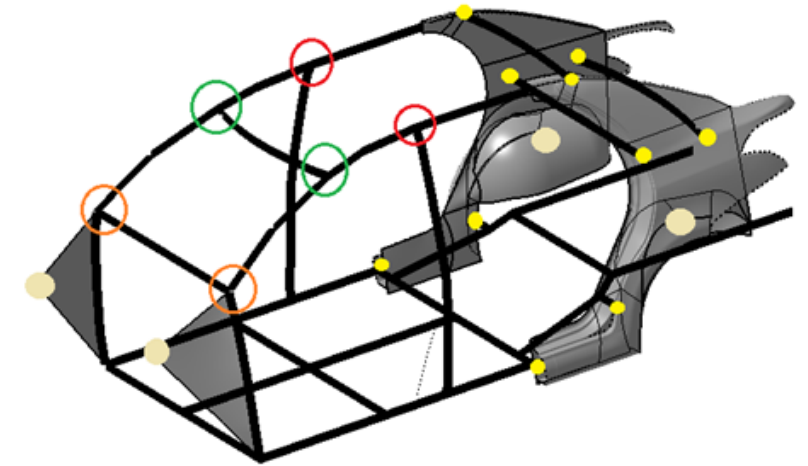
Dr. Isheng Yeh





Efficient non-linear beam models to replace detailed FE analysis for preliminary design

- CAE models for concept design
- Replace detailed FE model (shells, solids) by simple beam frame structure
- Complex structural behavior embedded in material model: \*MAT\_119 enhanced (IFLAG=2)



# LS-OPT<sup>®</sup>

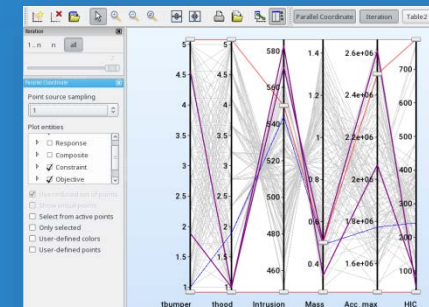
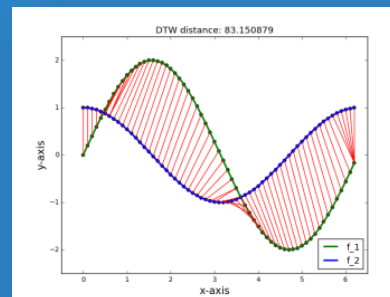
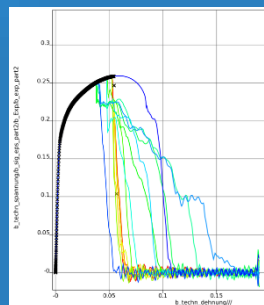
Dr. Nielen Stander<sup>1</sup>, Dr. Anirban Basudhar<sup>1</sup>, Imtiaz Gandikota<sup>1</sup>

Katharina Witowski<sup>2</sup>, Åke Svedin<sup>2</sup>, Charlotte Keisser<sup>2</sup>

Sophie Du Bois<sup>1</sup>, Denis Kirpicev<sup>1</sup>

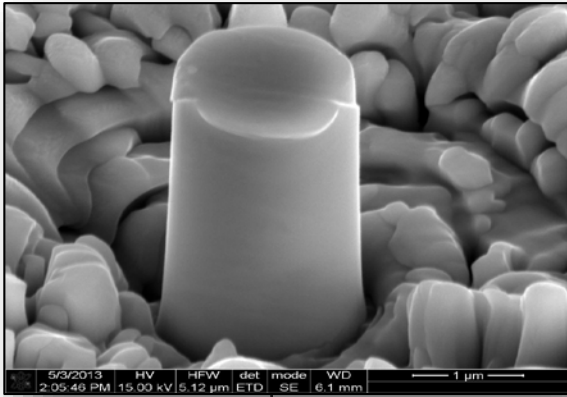
<sup>1</sup>Livermore Software Technology Corporation

<sup>2</sup>DYNAmore GmbH

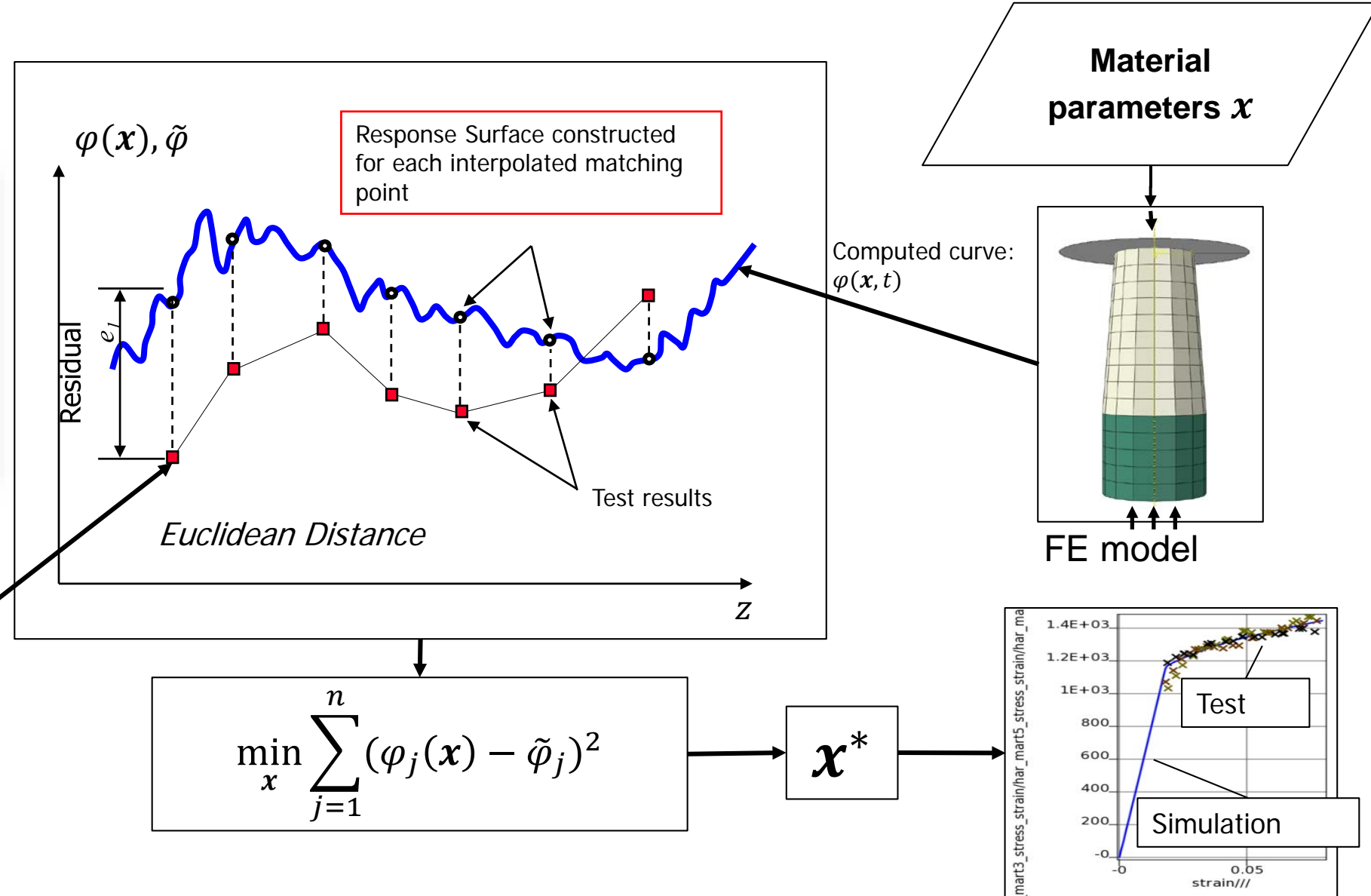
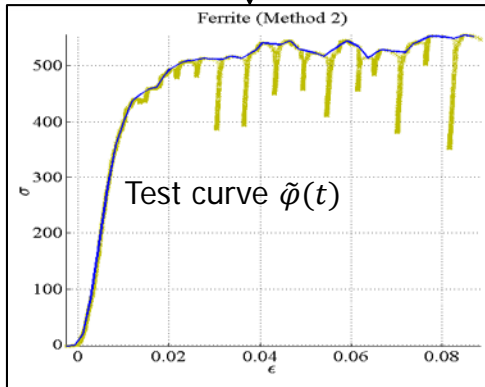


# Material Calibration: Introduction

Experiment (single crystal micropillar)

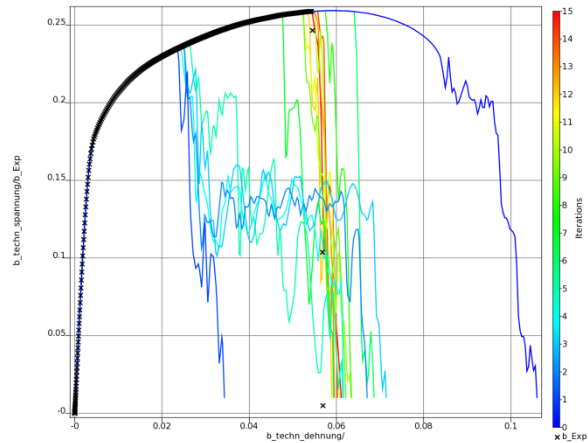


Result



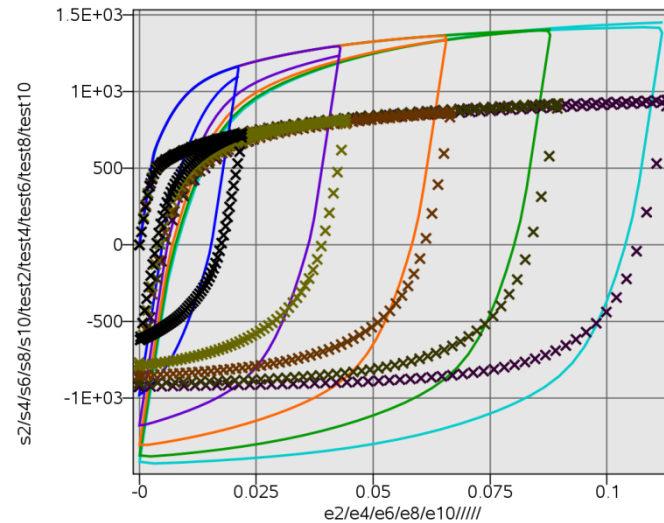
# Calibration | Computational challenges

Curve matching presents challenges due to the nature of the experimental or computational curves



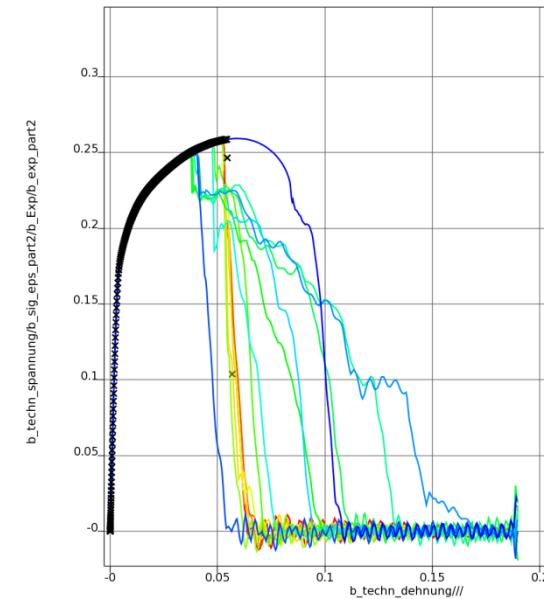
## Noise

Failure model:  
GISSMO — discrete process



## Hysteresis

Loading/Unloading  
Material 125



## Partial Matching

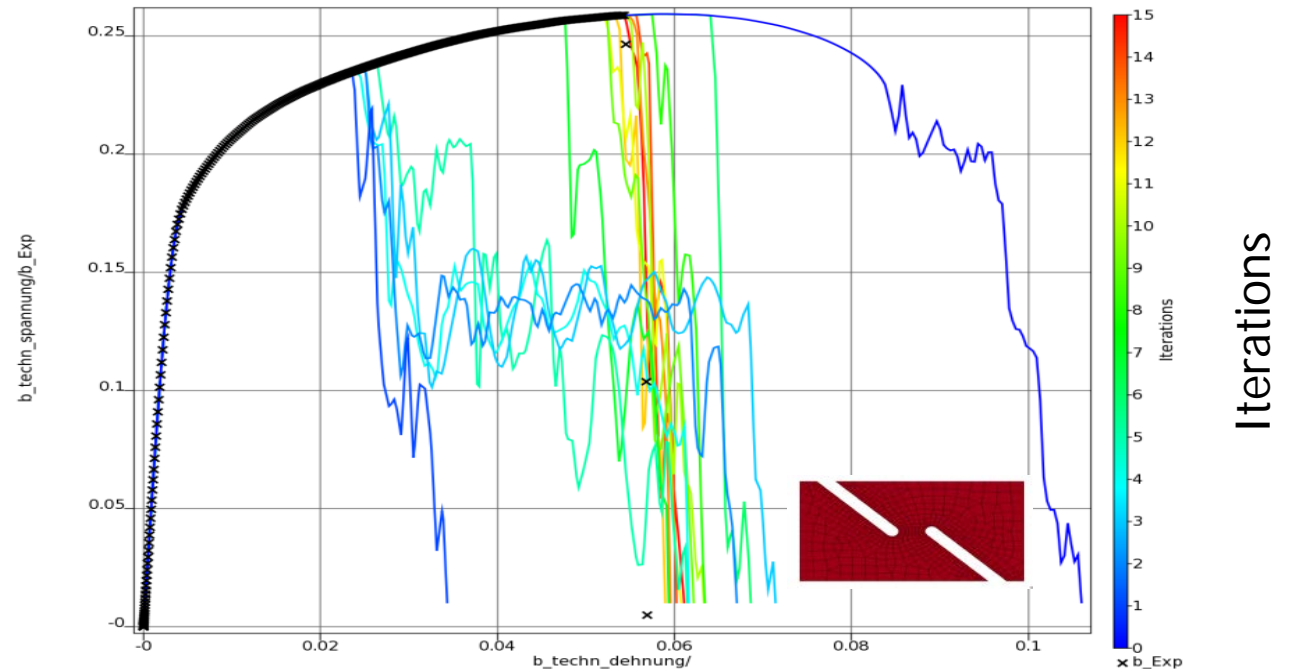
Failure model:  
GISSMO — oscillation after  
failure

# Example: GISSMO model

The GISSMO failure model requires special treatment for curve matching

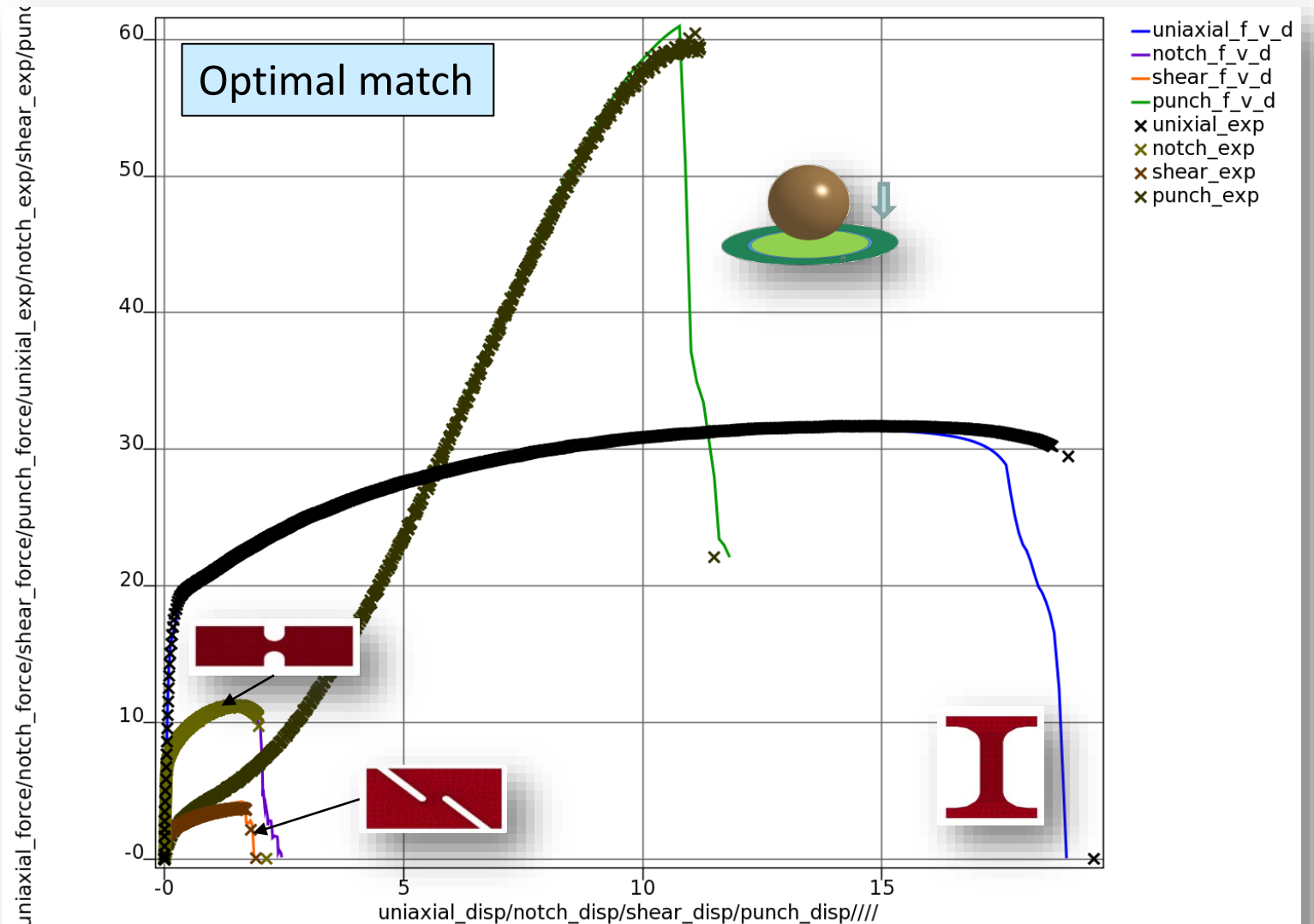
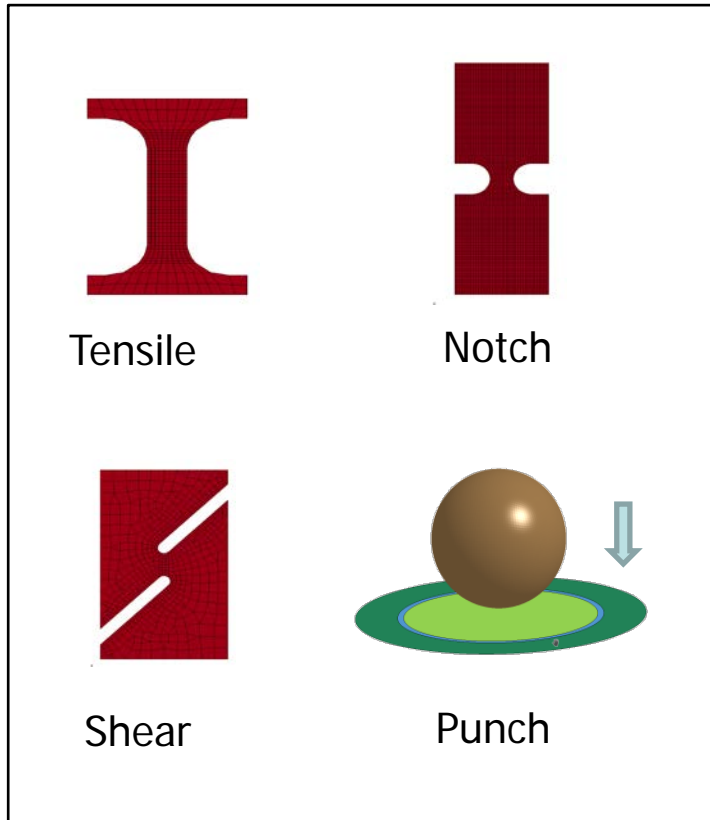
- Parameters: 7, Material Model: GISSMO
  - Uses discrete (element-by-element) erosion
- Curve Matching
  - Dynamic Time Warping (DTW)
  - Does not address partial curves  $\Rightarrow$  Truncate Force history at failure
- Optimization
  - SRSM (fast local optimizer)

## Shear: single case calibration history



# Calibration: GISSMO model

In industry, the calibration of the GISSMO model typically involves multiple cases





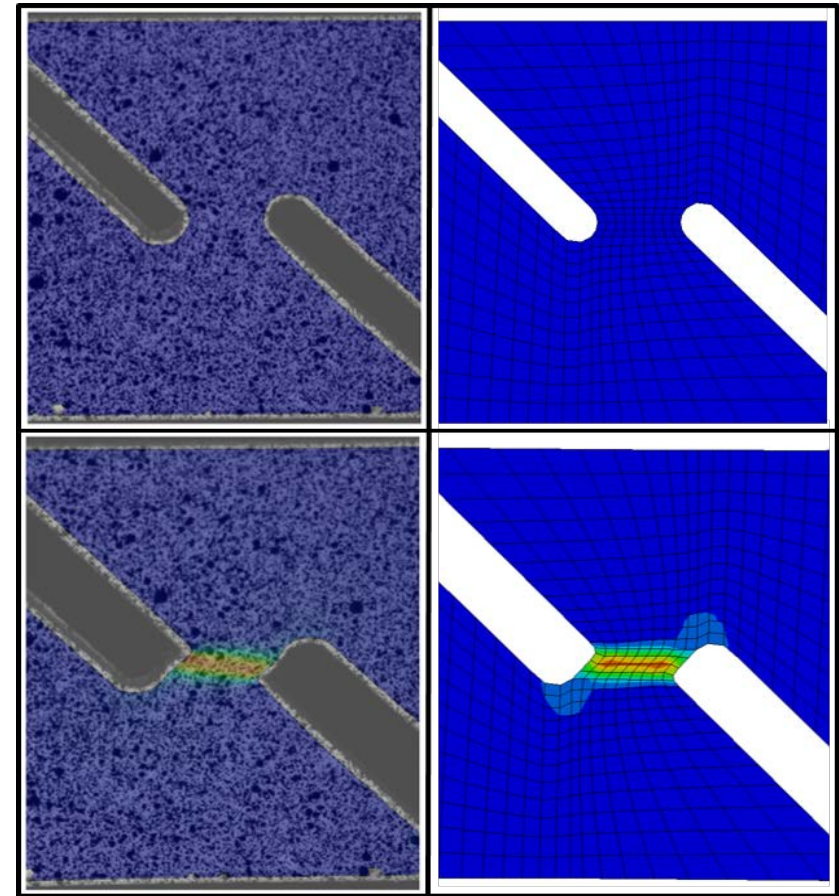
# Digital Image Correlation (DIC)

Optical method for tracking changes in images



Tensile testing  
equipment

Measurement  
system

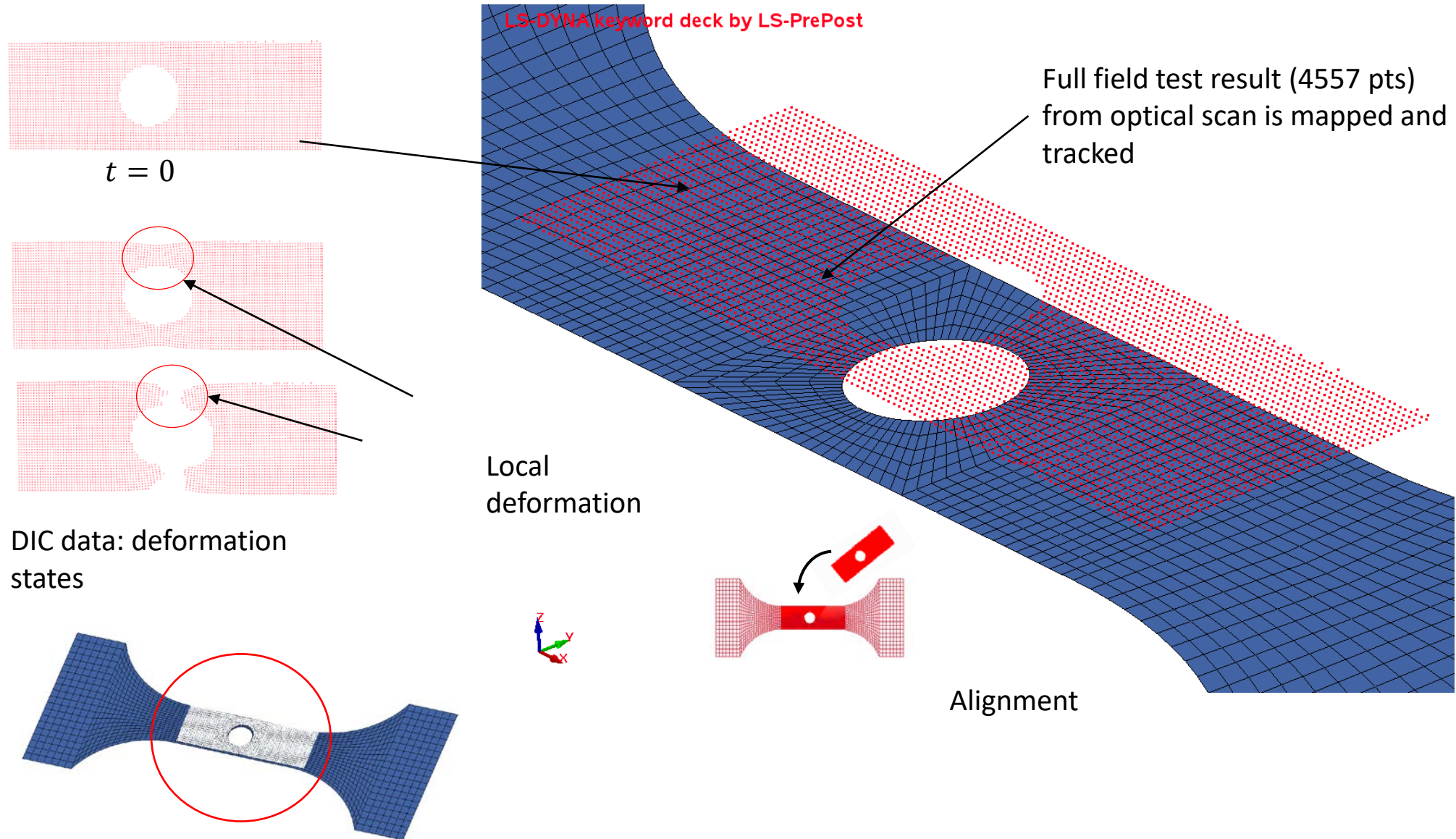


Experiment

Simulation

# DIC | Matching in time and space

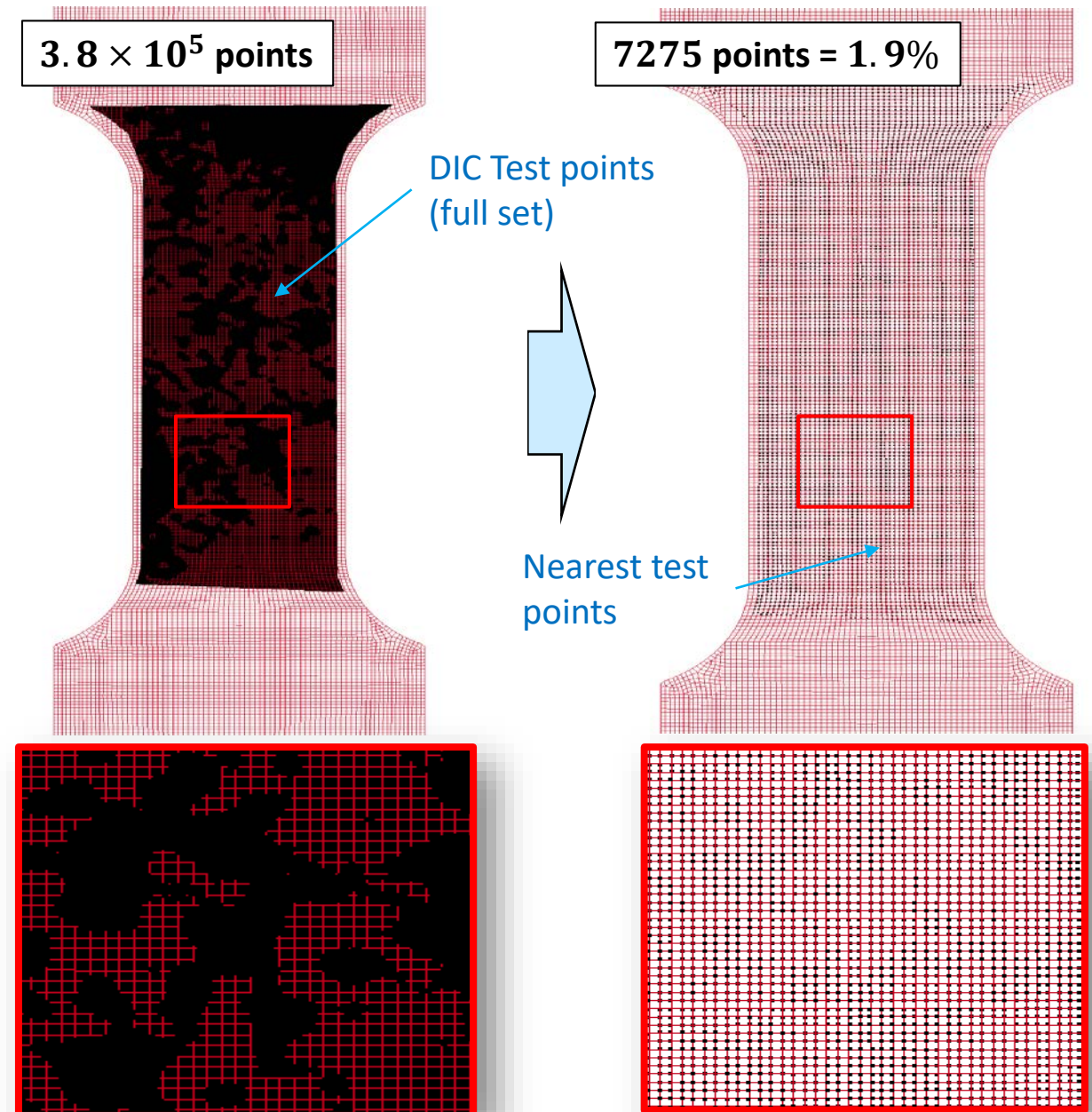
Test data can be mapped to the Finite Element model for Full-field calibration





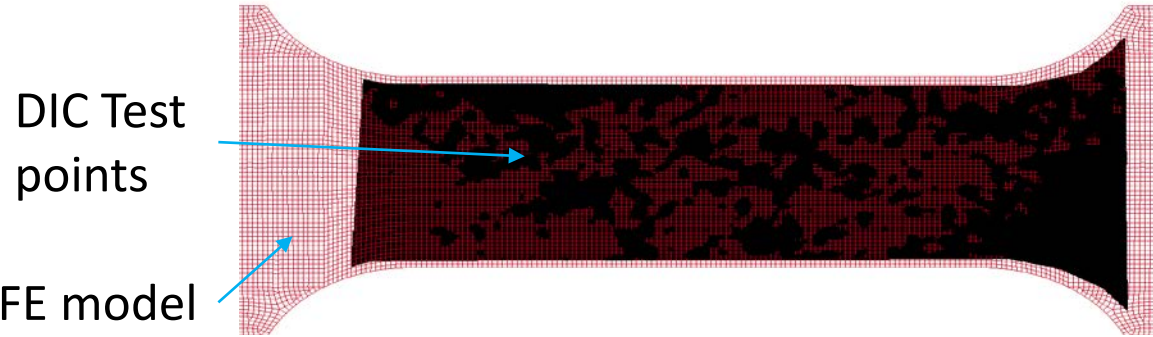
# Digital Image Correlation: *Nearest Neighbor Cluster*

- **Nearest Neighbor Clustering**
  - Pre-processing feature
  - Reduce resources for large point set ( $\sim 10^6$ )
    - Storage space
    - CPU time: mapping is done at each time step (vanishing nodes/points)
  - Nodal map
  - Can also apply a proximity tolerance for removing outlier points
- **Algorithm ( $t = 0$ )**
  - Nearest node to each point  $\rightarrow$  *reduced node set*.
  - Prune *reduced node set*  $\rightarrow$  *nearest points*
  - 1-to-1 map

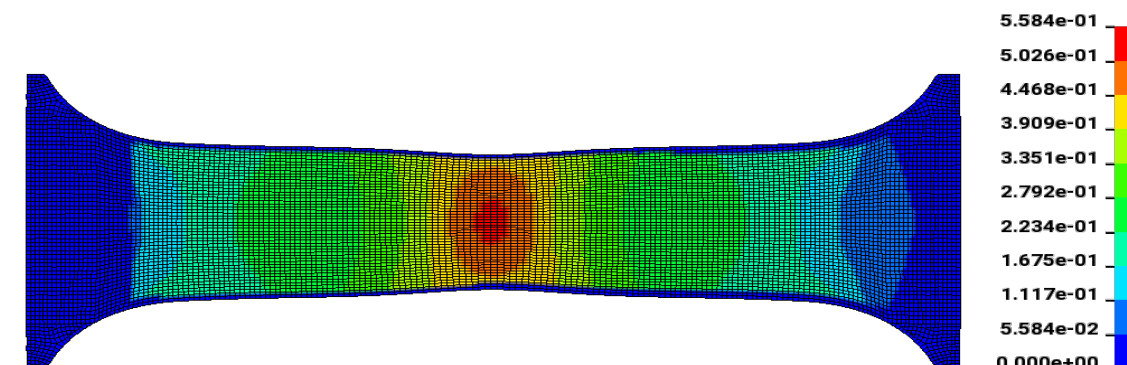
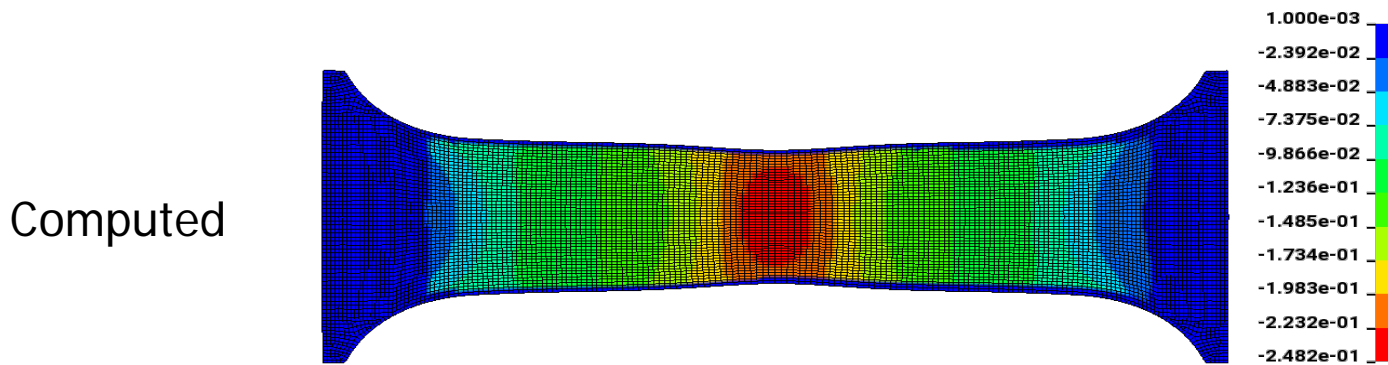
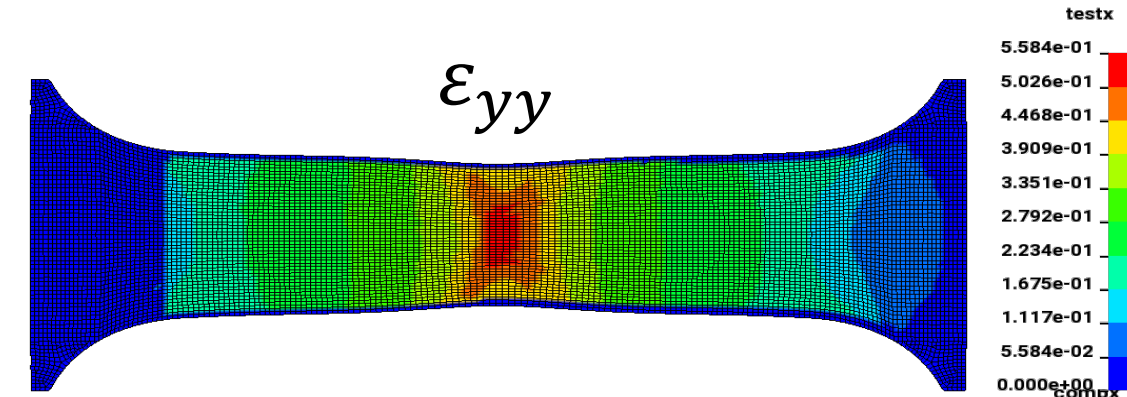
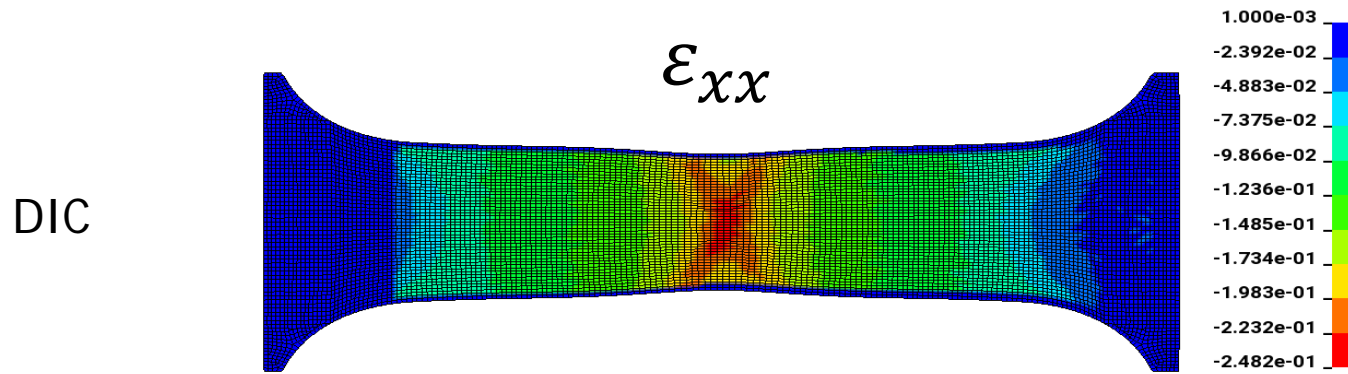


## Example 2: Tensile test

The contour comparison uses *Dynamic Time Warping*:  $3.8 \times 10^5$  DIC points

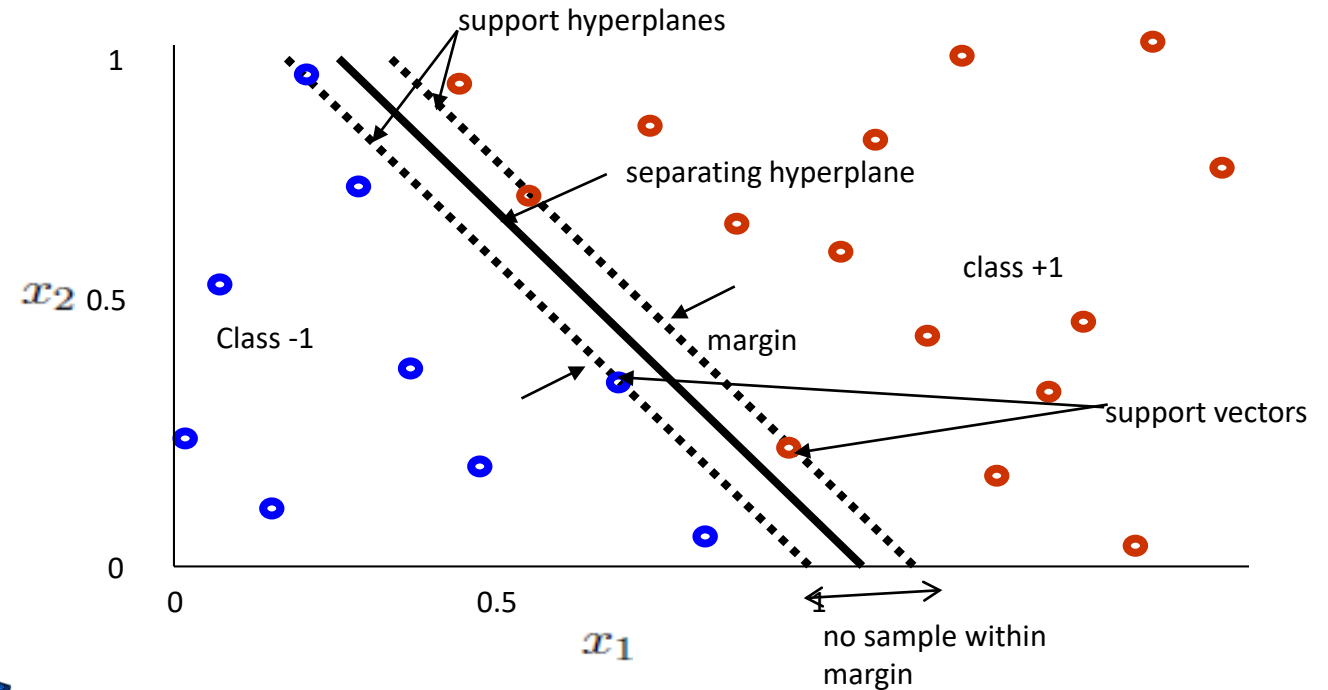
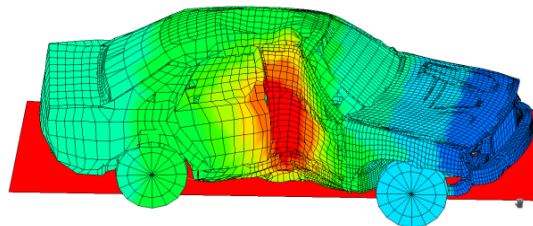
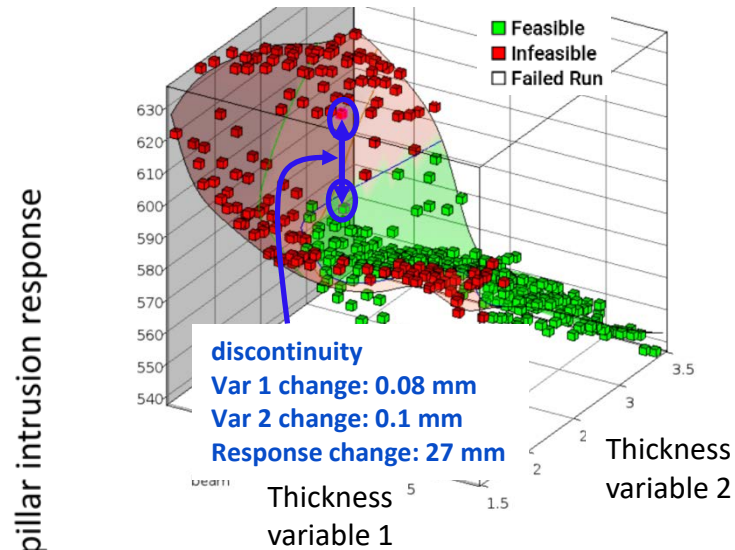


- Reduces 380,000 DIC points to 7275 points with nodal neighbors
- Reduces extraction time from 2 hours → 6 minutes



# Support Vector Machine Classification

- *Metamodel* approximation hampered by *discontinuities/noise*, hence global approximation using a metamodel may be inaccurate
- *Support Vector Machines (SVM)* treats the problem as a *classification* of feasible/infeasible patterns in the design space (instead of regression)

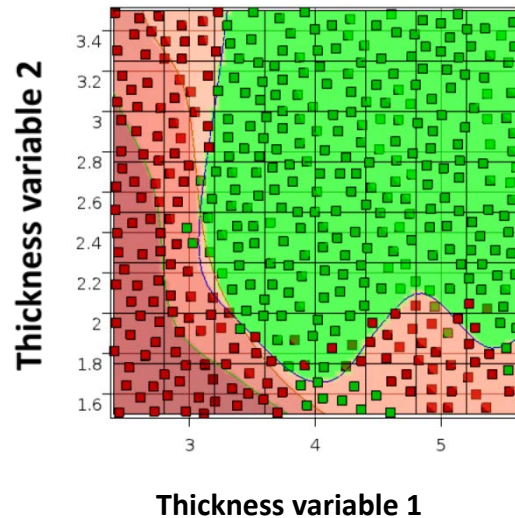


Optimal SVM maximizes the margin

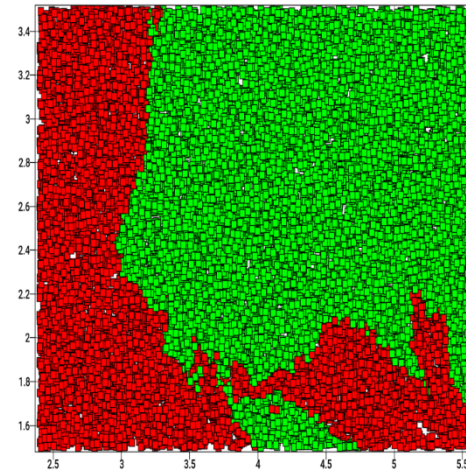


# Support Vector Machine Classification

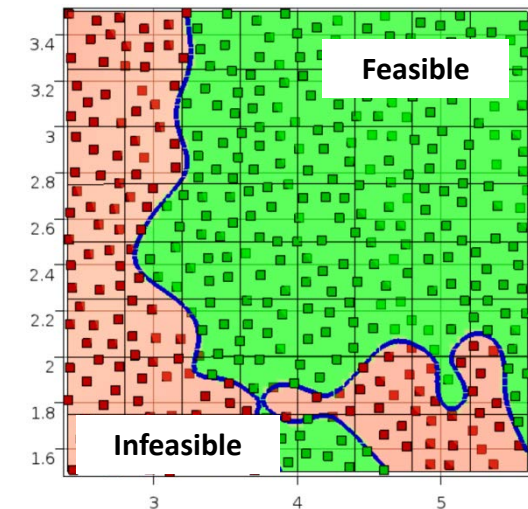
- Handles noisy and discontinuous/binary constraints
- Able to approximate highly nonlinear boundaries accurately
- Single classifier represents multiple constraints (allows computation savings)
- 3 intrusion constraints represented by a single SVM classifier (bottom right)



Neural Net approximation of constraint  
(**inaccurate**)



Actual constraint feasibility  
(LS-DYNA)



SVM Classifier  
(**accurate**)



# Summary

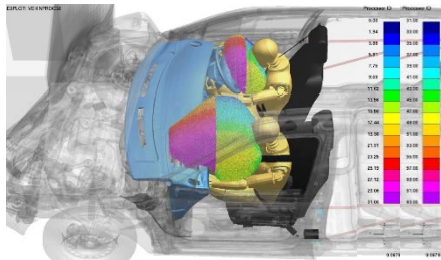
Our ultimate goal for the past two decades is the development of one highly scalable software, LS-DYNA, for large scale, multi-physics, full model, linear and nonlinear, static and transient, simulations in the engineering design process.

## Only one model is needed and created

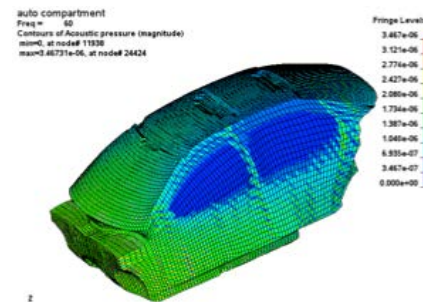
Multi-Physics and Multi-Stage  
Structure + Fluid + EM + Heat Transfer  
Implicit + Explicit ....

Multi-Scale  
Failure predictions, i.e., spot welds

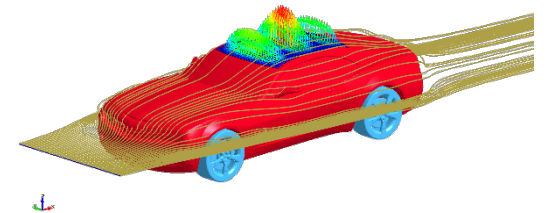
Multi-Formulations  
Linear + Non-Linear + Peridynamics + ...



Crash



NVH



Structure + Fluid



**LSTC**  
Livermore Software  
Technology Corp.

**DYNA**  
MORE

Announcement and Call for Papers

## 12<sup>th</sup> LS-DYNA EUROPEAN CONFERENCE & USERS MEETING

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14 - 16 May 2019 ■ Koblenz, Germany





**Thank you!**

LS-DYNA®

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Dummies & Barriers