# LS-DYNA for Mining and Mineral Processing Applications

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### **Outline**

- Rock drilling
- Stirred media mill

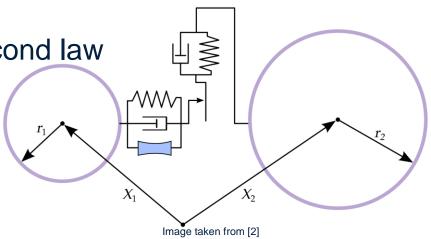


#### **Discrete Element Method**

Rigid spheres and Newton's second law

$$m_i \frac{d\boldsymbol{v}_i}{dt} = \boldsymbol{F_i}^{ext} + \sum_{j=1}^{n_j} \boldsymbol{F}_{ij}$$

- Penalty based contact
  - Normal and shear stiffness
- Friction
- Normal and shear damping





[2] Livermore Software Technology (2021). LS-Dyna Keyword User's Manual Volume 1 (R12)

<sup>[1]</sup> Cundall, P.A. and O.D.L. Strack (1979). A discrete numerical model for granular assemblies.

### **Bonded Discrete Element Method**

P1 Tension P2

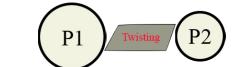
- Linear elastic beams connects spheres
- For each bond:
  - Normal and shear stiffness
  - Normal and shear strength

$$\Delta \bar{F}^n = \bar{k}^n A \Delta U^n$$

$$\Delta \bar{F}^s = -\bar{k}^s A \Delta U^s$$

$$\Delta \bar{M}^{\rm n} = -\bar{k}^{\rm s} J \Delta \theta^{\rm n}$$

$$\Delta \bar{M}^s = -\bar{k}^n I \Delta \theta^s$$



P1

Bond breaks once prescribed strength is exceeded

$$ar{\sigma}^{\max} = rac{-ar{F}^{\mathrm{n}}}{A} + rac{\left|ar{M}^{\mathrm{s}}\right|ar{R}}{I} \ge \sigma_{c}$$
 $ar{ au}^{\max} = rac{\left|ar{F}^{\mathrm{s}}\right|}{A} + rac{\left|ar{M}^{\mathrm{n}}\right|ar{R}}{I} \ge au_{c}$ 



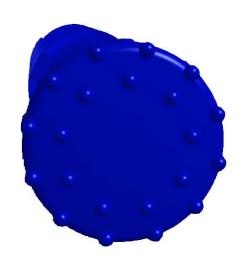
[3] Potyondy, D., Cundall, P (2004). A bonded-particle model for rock.

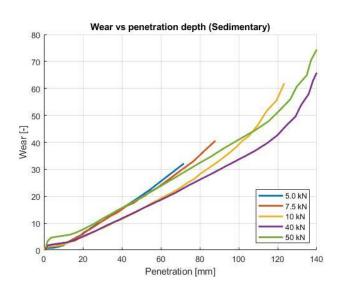
### **BDEM** and rock drilling



SMART GEOTHERMAL



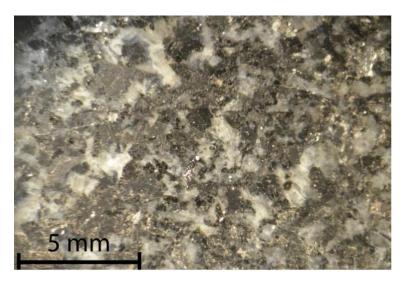






#### **Rock materials**

- Rock materials are heterogeneous
  - Different types of minerals
  - Varying grain sizes, shapes, boundaries and orientations
- Unpredictable material
  - Crack initiation and propagation
- How to model numerically?





### Heterogeneous rock model

Computational Particle Mechanics https://doi.org/10.1007/s40571-021-00434-w

#### Three steps in generating a rock body

Generation of grains with irregular sizes and shapes

2. Assigning BDEM properties of the grains

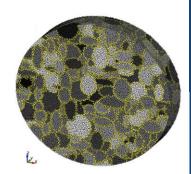
3. Cementing grains together

#### A statistical DEM approach for modelling heterogeneous brittle materials

Albin Wessling<sup>1</sup> ⊕ · Simon Larsson<sup>1</sup> · Pär Jonsén<sup>1</sup> · Jörgen Kajberg<sup>1</sup>

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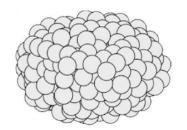




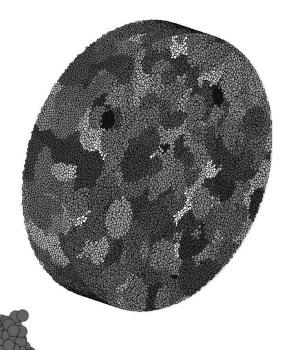
### Heterogeneous rock model: Grain generation

- Grains are represented by randomized ellipsoidal subsets of Bonded DEM
  - Uniform statistical distribution of ellipsoidal radii:

$$R_x$$
,  $R_y$ ,  $R_z \sim U(R_{\min}, R_{\max})$ 









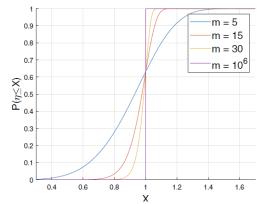
### Heterogeneous rock model: Grain properties

2. The <u>mean</u> bond stiffnesses and strengths of each grain is given by the Weibull distribution

$$f(\eta, \eta_0, \mathbf{m}) = \frac{\mathbf{m}}{\eta_0} \left(\frac{\eta}{\eta_0}\right)^{\mathbf{m} - 1} e^{-(\eta/\eta_0)^{\mathbf{m}}}$$

where m is the heterogeneity index

 Bond properties within one grain is allowed to vary within +/- 10 % of the mean value





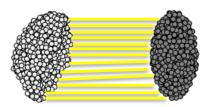
Color represents mean grain strength

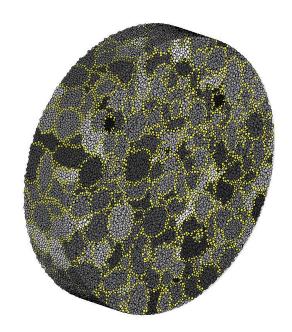
### Heterogeneous rock model: Cementing

3. A grain is cemented together with its neighbours with down-scaled bond strengths

$$\bar{\sigma}_c^{ij} = C_f \cdot \bar{\sigma}_c^i$$
$$\bar{\tau}_c^{ij} = C_f \cdot \bar{\tau}_c^i$$

Grain i Grain j

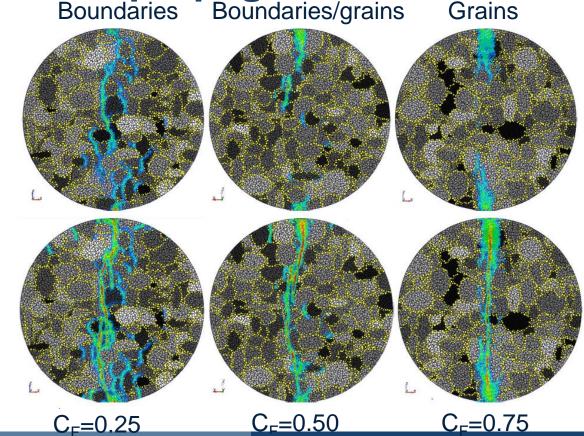




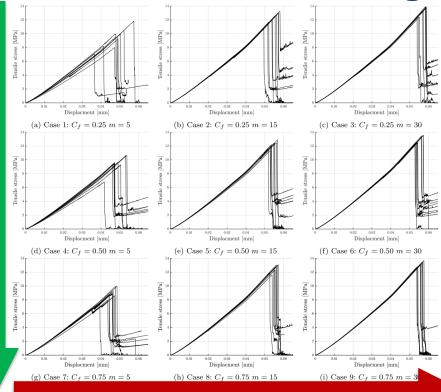
Results: crack propagation
Boundaries Boundaries/grains

Before main fracture

After main fracture



### **Predicted tensile strength**



Variation increases with decreased cement strength and heterogeinity index

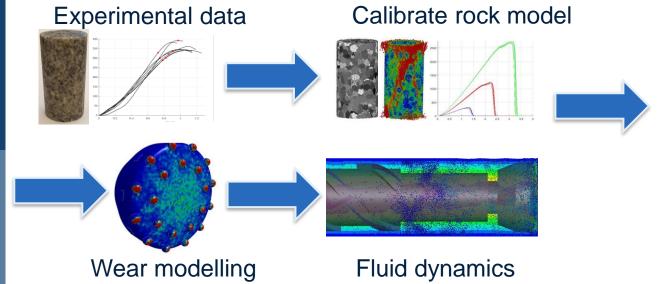
$$\sigma_t = \frac{2F}{\pi Dt}$$

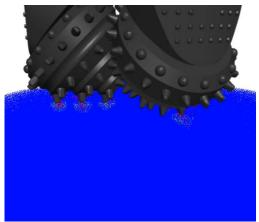
Heterogeneity index *m* 

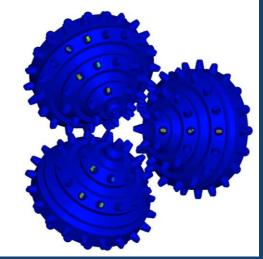
**Sement strength factor** 

### Ongoing work: DigiRock

**Aim:** Develop efficient and physically realistic numerical models for study and optimization of rock drilling







#### Stirred media mill

- Comminution in the minerals industry
  - Tumbling mills, low energy efficiency
  - Stirred media mills, higher energy efficiency
- Optimization of comminution in stirred media mills
- Modelling a wet-operating stirred media mill
  - Multiphysics in a complex system



#### **Materials**

#### Pilot wet stirred media mill

- Outotec HIG5
  - 7.5 kW
  - -6.21
  - 240 l/h



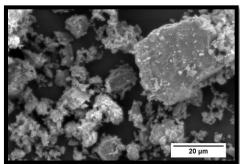


#### **Materials**

#### Grinding beads and feed material

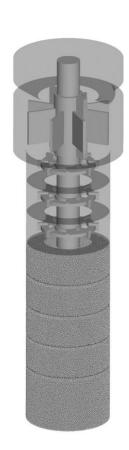
- Grinding beads
  - Composite alumina and zirconia ceramic
  - Spherical, 2.0 4.0 mm
- Feed material
  - Mineral powder + water
  - 46 % solids by weight





- FE-model
- DEM for grinding media
- Penalty-based coupled DEM-FEM







#### Slurry

Incompressible Computational Fluid Dynamics (ICFD)

Governing equations

$$\rho \left( \frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = -\frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j \partial x_j} + \rho f_i$$

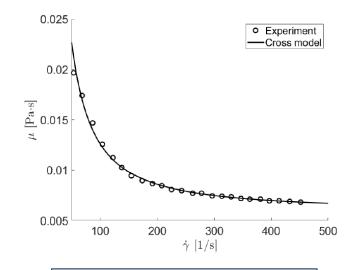
$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i}(\rho u_i) = 0 \qquad \qquad \frac{\partial u_i}{\partial x_i} = 0$$

- Model input
  - Constitutive model



## Slurry Constitutive model

- Newtonian/non-Newtonian?
  - Rheology suggests non-Newtonian
- Shear-thinning (Cross, 1965)

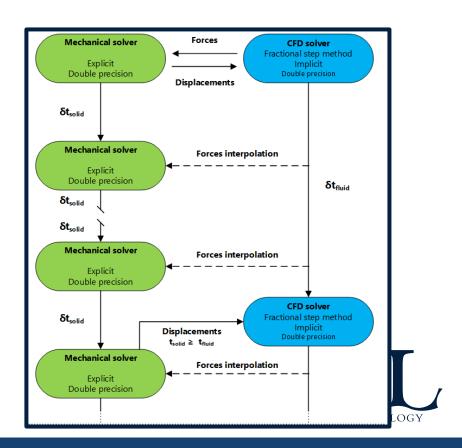


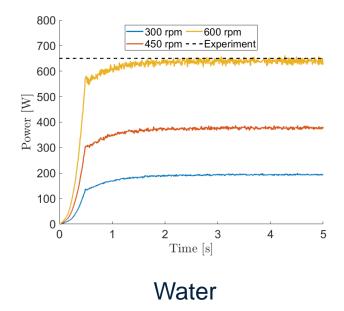
$$\mu = \mu_{\infty} + \frac{\mu_0 - \mu_{\infty}}{1 + (\lambda \dot{\gamma})^n}$$

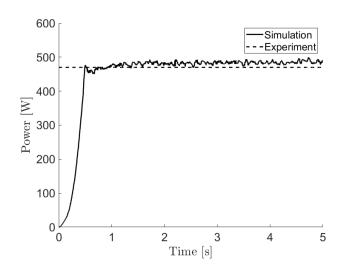
Cross, M. M. (1965). Rheology of non-Newtonian fluids: A new flow equation for pseudoplastic systems. *Journal of Colloid Science*, **20**, 417-437

#### Coupled ICFD-DEM-FEM

- Partitioned approach
- Loosely coupled
- Two-way coupling
- Drag force



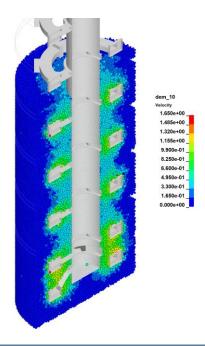


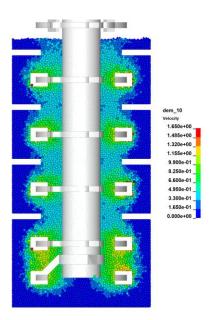


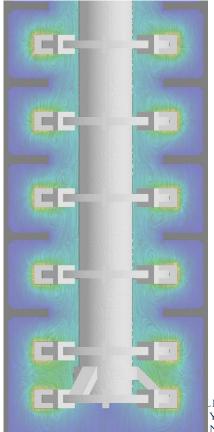
Mineral slurry



#### Grinding media and slurry dynamics

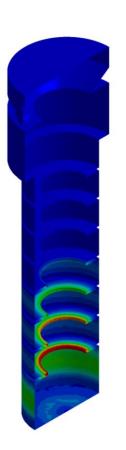


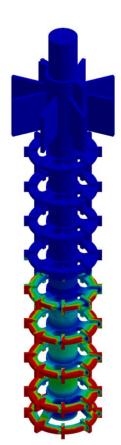


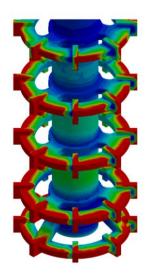




Wear

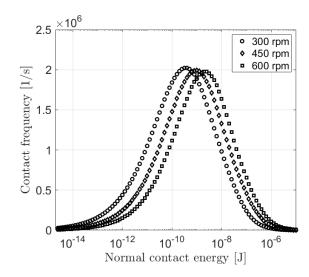




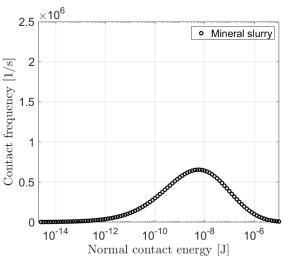




#### Contact energy spectra



Water



Mineral slurry



#### **Conclusions**

- Statistical rock model
  - Crack initiation, propagation and coalescence
  - Applicable in rock drilling
- Coupled ICFD-FEM-DEM models
  - Dynamics of grinding media and slurry
  - Power draw and wear
  - Interparticle collisions
  - Quantification of the comminution performance



#### **Questions**

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